



Canadian
Wood
Council

Conseil
canadien
du bois



Tall Walls Workbook

2007 Edition

***SINGLE STOREY COMMERCIAL
WOOD STRUCTURES***



Tall Walls Workbook 2007 Edition

A guide to designing
wood stud walls up to
11.9 m (39 ft) high for
single storey commercial
wood structures

***Canadian
Wood
Council***

***Conseil
canadien
du bois***

© 2007 Copyright
Canadian Wood Council
Conseil canadien du bois
99 Bank Street, Suite 400
Ottawa, Ontario, Canada
K1P 6B3
<http://www.cwc.ca/>

ISBN 0-921628-74-9

7.0M07-01

Photographs courtesy of:
Crestbrook Forest Industries
D.E. Schaefer Architect Ltd.

Printing:
Bonanza Printing & Copying Centre Inc.



Printed in Canada on recycled paper

Preface

In Canada, wood is well suited to commercial buildings of one to four storeys. The modifications to the fire resistance requirements in building codes and the development of stronger engineered wood products has expanded the permitted use of wood to longer spans with heavier loads. A new series of design publications has been produced to assist specifiers of larger commercial wood structures.

The Canadian Wood Council, together with national partners of the Wood WORKS! program, produced two workbooks, *Design and Costing Workbook* and *Tall Wall Workbook*, in 2000. The main goal of the *Design and Costing Workbook* was to provide detailed design and costing information for a single storey commercial building. The *Design and Costing Workbook* can be downloaded from www.cwc.ca, or ordered from the Canadian Wood Council at 1-800-463-5091.

The 2000 edition of the *Tall Wall Workbook* has been successfully used to assist in design of tall walls in commercial and industrial structures for the past six years. Stud design tables for both lumber and engineered wood studs are provided to demonstrate wood's suitability for engineered tall wall construction. The stud tables in this workbook are provided for lumber studs up to 6.1 m (20 ft.) and proprietary engineered wood studs up to 11.9 m (39 ft.). In addition, a detailed design example of manufacturing facility is provided describing structural, thermal and fire consideration for tall walls. This follow-up publication is addressing changes in the new edition of the National Building Code of Canada (NBCC 2005) and the CSA O86 Standard. The *Tall Wall Workbook* can be downloaded from www.cwc.ca.

The Canadian Wood Council has a complete set of publications and design tools to facilitate designing and building with wood. These include the *Wood Design Manual 2005*, referenced in the example, and the complete software for wood design, WoodWorks® Design Office. WoodWorks® Design Office includes SIZER, CONNECTIONS and SHEAR-WALLS to assist in the design process. A working demonstration of the software can be viewed at www.woodworks-software.com/.

In addition to structural and economic factors, environmental concerns increasingly play a role in construction project decision making. In this area, wood has the following advantages:

- Wood is the only major building material that is renewable
- The volume of wood in Canada's commercial forests has increased over the past 20 years
- Wood produces less pollution during manufacturing and use than any other building material
- Wood provides superior energy savings because of its thermal performance.

Every effort has been made to ensure the data and information in this publication are as accurate as possible. The Canadian Wood Council does not, however, assume any responsibility for errors or omissions in the publication nor for any designs or plans prepared from it.

For more information, contact the Canadian Wood Council at 1-800-463-5091.

Table of Contents

1.0	Introduction	1
2.0	Stud Tables	3
2.1	Lumber Studs for wind pressure $q_{50} = 0.65$ kPa	5
2.2	Lumber Studs for wind pressure $q_{50} = 0.55$ kPa	8
2.3	Lumber Studs for wind pressure $q_{50} = 0.45$ kPa	11
2.4	VERSA-STUD® by BOISE for wind pressure $q_{50} = 0.65$ kPa	14
2.5	VERSA-STUD® by BOISE for wind pressure $q_{50} = 0.55$ kPa	16
2.6	VERSA-STUD® by BOISE for wind pressure $q_{50} = 0.45$ kPa	18
2.7	LP LVL Studs - Louisiana-Pacific for wind pressure $q_{50} = 0.65$ kPa	20
2.8	LP LVL Studs - Louisiana-Pacific for wind pressure $q_{50} = 0.55$ kPa	22
2.9	LP LVL Studs - Louisiana-Pacific for wind pressure $q_{50} = 0.45$ kPa	24
2.10	Nordic Lam Wall Studs for wind pressure $q_{50} = 0.65$ kPa	26
2.11	Nordic Lam Wall Studs for wind pressure $q_{50} = 0.55$ kPa	28
2.12	Nordic Lam Wall Studs for wind pressure $q_{50} = 0.45$ kPa	30
2.13	Temlam Studs by Jager EWP for wind pressure $q_{50} = 0.65$ kPa	32
2.14	Temlam Studs by Jager EWP for wind pressure $q_{50} = 0.55$ kPa	34
2.15	Temlam Studs by Jager EWP for wind pressure $q_{50} = 0.45$ kPa	36
3.0	Example	38
3.1	Overview of building	38
3.2	Stud Design	39
3.3	Stud Connection Design	48
3.4	Shearwall Design	51
3.4.1	Lateral Load Path and Overturning	51
3.4.2	Shear Panel Design	54
3.4.3	Chord Design	54
3.4.4	Anchor Bolt Design	56
3.4.5	Drag Strut Design	58
3.5	Design of Members and Connections Around the Wall Opening	60
3.5.1	Lintel Member and Connection Design	60
3.5.2	Jack Post Stud Design	63
3.5.3	King Post Member and Connection Design	63
3.6	Non-structural considerations	65
3.6.1	Fire Resistance Rating	65
3.6.2	Thermal Resistance	65



1. Introduction

This Workbook is intended to assist in using wood for the design of tall walls in commercial and industrial structures and to provide a step-by-step guide to the design of these walls. The popularity of single storey commercial projects, coupled with the wide availability of wood in Canada presents designers with many opportunities to use wood economically in these applications. Stud design tables for both lumber and engineered wood studs and a design example are provided to assist designers in specifying wood products in engineered tall wall construction.

The engineered tall walls described in this Workbook are extensions of the traditional stud walls used in Canada for over a hundred years. The traditional stud wall has proven to be such a successful construction technique because:

- The wood studs and framing can efficiently resist the snow loads on the roof and the wind loads on the wall and remove the need for an additional load bearing frame.
- When sheathing is added to the studs, the wall is very effective in resisting the lateral racking loads caused by wind and earthquakes.
- The walls can be easily insulated to provide excellent thermal resistance.
- Wood stud walls are readily finished with a wide range of finishing materials.
- Stud walls can be modified to adapt to the changing needs of the building.

The same rationale that has made the traditional stud wall so successful can be applied to the taller stud walls required for commercial structures. Larger lumber sizes or engineered wood products can be used to obtain the same wall strength in taller and longer walls. Shearwalls and connections can readily be designed to provide the required lateral resistance. Thermal requirements can be easily achieved with tall stud walls. By paying attention to details and selecting the correct finishing materials, tall stud walls can meet the more stringent fire and acoustical separation requirements for most commercial structures.

This publication is a design tool for tall walls used in single storey commercial structures. This Workbook includes:

- Stud tables for building a tall wall out of wood studs.
- A step by step design example for a tall wall to assist in designs.

This Workbook is subdivided as follows:

- 1. INTRODUCTION** gives background information.
- 2. STUD TABLES** are provided for lumber studs up to 6.1 m (20 ft) and proprietary engineered wood studs up to 11.9 m (39 ft). These stud tables are intended for use in tall wood stud walls for a given application. In a commercial application, a fully engineered design is required for each tall wall to consider the specific design considerations for that site, the connections and the other details required. In addition to the stud wall tables presented in the Workbook, www.cwc.ca contains the easy to use TallWALL sizer.
- 3. EXAMPLE** provides a detailed design example of a 7.72 m (25 ft 4 in) tall wall using the Crestbrook Value Added Centre in Cranbrook, BC. References are noted as follows:



Wood Design Manual 2005



CSA O86.1–01 Engineering Design in Wood (Limit States Design) and 2005 Supplement



National Building Code of Canada 2005



User's Guide – NBC 2005 Structural Commentaries (Part 4)

The design example features stud and connection design, shearwall design, design around wall openings and wall requirements for thermal resistance and fire resistance rating.

Wood structures offer many advantages for commercial and industrial buildings. This publication will allow the user to quickly evaluate a wood option for their projects. In addition, wood construction offers a range of advantages that include the following:

- Competitive material costs
- Availability of labour
- Ease of installation and material handling
- Shortened construction schedules
- Finishing options
- Ability to create complex building shapes with relative ease
- Increased thermal performance and energy efficiency
- Use of the most sustainable, environmentally friendly building product.

2. Stud Tables

Scope

This section features stud tables for lumber studs and proprietary engineered wood studs. These stud tables are intended for using tall wood stud walls for a given application. In a commercial building, a fully engineered design is required for each tall wall to consider the specific design considerations for that site, the effect of openings, the connections and other details. A full design example for a tall wall is given in Section 3.

Assumptions Used to Develop the Stud Tables

- The studs are laterally braced to prevent buckling in the narrow dimension.
- The loads are uniformly distributed along the top of the wall.
- The 1/50 hourly wind pressure ($q_{1/50}$) specified wind loads have been modified by the following coefficients:

$$C_e = 0.7$$

$$C_p C_g = -2.0$$

$$C_{pi} = 0.3$$

$$C_{gi} = 2.0$$

- The 1/50 hourly wind pressures ($q_{1/50}$) is used in strength and deflection calculations.
- Total load deflection criteria is stud length/180. Calculated total load deflection for each stud is given in the Tables.
- The ratio of specified axial dead load to live load is 1. The tables can be used conservatively when the specified axial dead load is less than the specified axial live load.
- Stud sizes are based on Limit State Design. The Limit State Design load combinations considered are:
 1. axial load alone
 2. wind plus axial load, where wind is the principal load and snow is the companion load
 3. wind plus axial load, where snow is the principal load and wind is the companion load

- Load cases 2 and 3 are considered short term load
- Eccentric axial loading of the stud is considered with maximum eccentricity equal to 1/6th of the stud depth.
- The Moment Magnifier Method is used to account for the secondary bending moment ($P\Delta$) effect.
- Deflections from wind and eccentric axial loads are amplified to account for the $P\Delta$ effect.
- Studs are pinned at both ends.
- The tables can only be used for untreated studs in dry service conditions.
- Normal importance category is assumed. Importance factors used are: $I_w = 1.0$ for ultimate limit state use, and $I_w = 0.75$ for serviceability limit state use. If a building falls under “Low” or “High” importance category, it is suggested that the designer chooses a corresponding higher (or lower) wind load.
- No notching or drilling of the studs is allowed.

For the lumber stud tables:

- Resistance values were calculated based on CSA Standard O86.1-01 and the 2005 Supplement.
- A “Case 2” load sharing system, as defined in CSA O86.1-01, is assumed. In order to meet this requirement, the studs must be sheathed with plywood, waferboard, or OSB of minimum 9.5 mm thickness and attached to the studs to provide a minimum stiffness equivalent to that provided by 2-inch common nails at 150 mm centres at edges of sheathing panels and 300 mm centres elsewhere.

How to Use the Tables

- Determine the $q_{1/50}$ Hourly Wind Pressures for the building location. This is found in the Climatic Data Section of the *National Building Code* or the appropriate Provincial Building Code.
- Calculate the specified uniformly distributed dead load based on materials supported. Consideration is to be given to the self weight of the wall. Under many conditions it is appropriate to include the weight of the top half of the wall.
- Calculate the specified uniformly distributed live load based on specified loads due to snow and associated rain in the Building Code and tributary width of roof.
- The stud tables are appropriate for the typical case where the specified axial dead load does not exceed the specified axial live load.
- Calculate the factored uniformly distributed load $(1.25D + 1.5S)$ kN/m along the stud wall.
- Select the table(s) for the stud material(s) being considered. The table(s) selected should have $q_{1/50}$ wind loads which are greater than or equal to the climatic data for the building site.
- Based on the length of the stud, the spacing of the stud and the axial load, select a stud depth. The associated deflection should be considered for appropriateness where finishes are susceptible to cracking.



Table 2.1 - Lumber Studs

Wind pressure $q_{1/50}$ 0.65 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		S-P-F No. 2 Grade (or better)					D.Fir-L No. 2 Grade (or better)				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/444	L/281	L/187	L/305	L/222	L/516	L/327	L/218	L/354	L/258
	20	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/413	L/261	L/410	L/289	L/210	L/482	L/305	L/204	L/337	L/245
	30	Depth	140	140	184	184	184	140	140	184	184	184
		Deflection	L/384	L/243	L/388	L/273	L/198	L/450	L/286	L/453	L/320	L/233
	40	Depth	140	140	184	184	184	140	140	184	184	235
		Deflection	L/357	L/225	L/367	L/259	L/187	L/420	L/267	L/430	L/304	L/479
	50	Depth	140	140	184	184	235	140	140	184	184	235
		Deflection	L/333	L/209	L/348	L/245	L/393	L/394	L/250	L/409	L/289	L/460
406	10	Depth	140	140	184	184	235	140	140	184	184	184
		Deflection	L/330	L/208	L/323	L/227	L/349	L/384	L/242	L/375	L/264	L/192
	20	Depth	140	140	184	184	235	140	140	184	184	235
		Deflection	L/304	L/191	L/303	L/212	L/332	L/355	L/224	L/354	L/249	L/387
	30	Depth	140	184	184	184	235	140	184	184	235	235
		Deflection	L/280	L/421	L/284	L/199	L/316	L/329	L/491	L/333	L/502	L/369
	40	Depth	140	184	184	235	235	140	184	184	235	235
		Deflection	L/258	L/395	L/267	L/409	L/301	L/305	L/463	L/314	L/478	L/352
	50	Depth	140	184	184	235	235	140	184	184	235	235
		Deflection	L/237	L/371	L/251	L/389	L/286	L/283	L/436	L/297	L/456	L/337
610	10	Depth	140	184	184	235	235	140	184	184	235	235
		Deflection	L/216	L/316	L/212	L/316	L/230	L/252	L/368	L/247	L/367	267.722
	20	Depth	140	184	184	235	235	184	184	235	235	286
		Deflection	L/195	L/293	L/196	L/297	L/217	L/535	L/342	L/489	L/346	461.807
	30	Depth	184	184	235	235	286	184	184	235	235	286
		Deflection	L/423	L/271	L/394	L/279	L/377	L/495	L/318	L/460	L/327	439.746
	40	Depth	184	235	235	235	286	184	235	235	286	286
		Deflection	L/391	L/538	L/370	L/263	L/358	L/459	L/629	L/434	L/565	419.093
	50	Depth	235	235	235	286	286	184	235	235	286	286
		Deflection	L/755	L/505	L/349	L/459	L/341	L/427	L/591	L/410	L/537	L/400

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.1 (continued) - Lumber Studs

Wind pressure $q_{1/50}$ 0.65 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		Hem-Fir No. 2 Grade (or better)					Northern Species No. 2 Grade (or better)				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	184	184	140	140	184	184	235
		Deflection	L/516	L/327	L/218	L/354	L/258	L/324	L/204	L/317	L/223	L/343
	20	Depth	140	140	140	184	184	140	140	184	184	235
		Deflection	L/482	L/305	L/204	L/337	L/245	L/298	L/187	L/297	L/208	L/326
	30	Depth	140	140	140	184	184	140	184	184	235	235
		Deflection	L/450	L/286	L/190	L/320	L/233	L/274	L/413	L/279	L/422	L/310
	40	Depth	140	140	184	184	184	140	184	184	235	235
		Deflection	L/420	L/267	L/430	L/304	L/221	L/252	L/387	L/262	L/401	L/295
	50	Depth	140	140	184	184	235	184	184	235	235	235
		Deflection	L/394	L/250	L/409	L/289	L/460	L/556	L/363	L/532	L/382	L/281
406	10	Depth	140	140	184	184	184	140	184	184	235	235
		Deflection	L/384	L/242	L/375	L/264	L/192	L/240	L/351	L/235	L/350	L/255
	20	Depth	140	140	184	184	235	140	184	184	235	235
		Deflection	L/355	L/224	L/354	L/249	L/387	L/218	L/326	L/219	L/330	L/241
	30	Depth	140	140	184	184	235	184	184	235	235	286
		Deflection	L/329	L/207	L/333	L/234	L/369	L/471	L/302	L/438	L/311	L/419
	40	Depth	140	184	184	235	235	184	184	235	235	286
		Deflection	L/305	L/463	L/314	L/478	L/352	L/436	L/281	L/413	L/294	L/399
	50	Depth	184	184	184	235	235	235	235	235	286	286
		Deflection	L/664	L/436	L/297	L/456	L/337	L/839	L/562	L/389	L/511	L/380
610	10	Depth	140	184	184	235	235	184	184	235	286	286
		Deflection	L/252	L/368	L/247	L/367	L/268	L/364	L/230	L/327	L/419	L/306
	20	Depth	140	184	235	235	235	184	235	235	286	N/A
		Deflection	L/229	L/342	L/489	L/346	L/253	L/332	L/449	L/305	L/393	N/A
	30	Depth	184	184	235	235	286	184	235	286	286	N/A
		Deflection	L/495	L/318	L/460	L/327	L/440	L/303	L/417	L/518	L/370	N/A
	40	Depth	184	184	235	235	286	286	286	286	N/A	N/A
		Deflection	L/459	L/296	L/434	L/309	L/419	L/1034	L/696	L/486	N/A	N/A
	50	Depth	235	235	235	286	286	N/A	N/A	N/A	N/A	N/A
		Deflection	L/881	L/591	L/410	L/537	L/400	N/A	N/A	N/A	N/A	N/A

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.1 (continued) - MSR Lumber Studs

Wind pressure $q_{1/50}$ 0.65 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		Grade 1650f-1.5E					Grade 2100f-1.8E				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/483	L/305	L/204	L/331	L/241	L/584	L/369	L/247	L/401	L/292
	20	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/449	L/285	L/190	L/314	L/229	L/546	L/347	L/232	L/382	L/278
	30	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/419	L/265	L/422	L/298	L/217	L/511	L/326	L/217	L/364	L/265
	40	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/391	L/248	L/401	L/283	L/205	L/479	L/306	L/203	L/347	L/253
	50	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/365	L/231	L/380	L/268	L/194	L/450	L/287	L/190	L/330	L/240
406	10	Depth	140	140	184	184	235	140	140	140	184	184
		Deflection	L/359	L/226	L/351	L/246	L/379	L/435	L/274	L/183	L/298	L/217
	20	Depth	140	140	184	184	235	140	140	184	184	184
		Deflection	L/331	L/208	L/330	L/232	L/361	L/404	L/255	L/401	L/282	L/205
	30	Depth	140	140	184	184	235	140	140	184	184	184
		Deflection	L/306	L/192	L/310	L/218	L/344	L/375	L/237	L/379	L/267	L/194
	40	Depth	140	184	184	184	235	140	140	184	184	184
		Deflection	L/283	L/431	L/292	L/205	L/328	L/349	L/220	L/359	L/252	L/182
	50	Depth	140	184	184	184	235	140	140	184	184	235
		Deflection	L/261	L/405	L/275	L/192	L/313	L/325	L/204	L/339	L/239	L/384
610	10	Depth	140	184	184	235	235	140	184	184	184	235
		Deflection	L/235	L/344	L/231	L/343	L/250	L/286	L/416	L/280	L/196	L/303
	20	Depth	140	184	184	235	235	140	184	184	184	235
		Deflection	L/213	L/319	L/214	L/323	L/236	L/261	L/388	L/261	L/183	L/287
	30	Depth	140	184	184	235	235	140	184	184	235	235
		Deflection	L/193	L/296	L/198	L/305	L/222	L/239	L/362	L/244	L/372	L/272
	40	Depth	184	184	184	235	235	140	184	184	235	235
		Deflection	L/427	L/275	L/184	L/288	L/210	L/219	L/339	L/228	L/352	L/258
	50	Depth	235	235	235	235	235	184	184	184	235	235
		Deflection	L/822	L/550	L/381	L/271	L/198	L/487	L/317	L/213	L/334	L/245

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.2 - Lumber Studs

Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		S-P-F No. 2 Grade (or better)					D.Fir-L No. 2 Grade (or better)				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/521	L/330	L/220	L/359	L/261	L/605	L/383	L/257	L/417	L/304
	20	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/480	L/305	L/203	L/338	L/246	L/560	L/356	L/238	L/394	L/288
	30	Depth	140	140	140	184	184	140	140	140	184	184
Deflection		L/443	L/282	L/187	L/318	L/231	L/519	L/331	L/221	L/373	L/272	
40	Depth	140	140	184	184	184	140	140	184	184	184	
	Deflection	L/410	L/260	L/424	L/300	L/218	L/482	L/308	L/497	L/353	L/257	
50	Depth	140	140	184	184	184	140	140	184	184	235	
	Deflection	L/380	L/241	L/399	L/283	L/204	L/449	L/287	L/470	L/334	L/531	
406	10	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/387	L/244	L/379	L/267	L/194	L/450	L/285	L/190	L/310	L/226
	20	Depth	140	140	184	184	184	140	140	184	184	184
		Deflection	L/353	L/223	L/354	L/249	L/180	L/413	L/261	L/413	L/291	L/211
	30	Depth	140	140	184	184	235	140	140	184	184	235
Deflection		L/323	L/203	L/330	L/232	L/368	L/380	L/240	L/387	L/273	L/430	
40	Depth	140	184	184	184	235	140	184	184	235	235	
	Deflection	L/295	L/453	L/308	L/216	L/348	L/350	L/531	L/363	L/552	L/408	
50	Depth	140	184	184	235	235	140	184	184	235	235	
	Deflection	L/270	L/423	L/288	L/447	L/330	L/322	L/498	L/341	L/524	L/388	
610	10	Depth	140	184	184	235	235	140	184	184	235	235
		Deflection	L/253	L/371	L/249	L/371	L/271	L/295	L/431	L/290	L/431	L/315
	20	Depth	140	184	184	235	235	140	184	184	235	235
		Deflection	L/227	L/340	L/229	L/346	L/253	L/267	L/398	L/268	L/404	L/296
	30	Depth	184	184	235	235	235	184	184	235	235	286
Deflection		L/485	L/313	L/455	L/324	L/237	L/568	L/368	L/532	L/380	L/511	
40	Depth	184	184	235	235	286	184	184	235	235	286	
	Deflection	L/445	L/288	L/426	L/304	L/414	L/523	L/340	L/499	L/357	L/484	
50	Depth	235	235	235	235	286	184	235	235	286	286	
	Deflection	L/846	L/572	L/398	L/285	L/392	L/483	L/670	L/468	L/614	L/459	

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.2 (continued) - Lumber Studs

Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		Hem-Fir No. 2 Grade (or better)					Northern Species No. 2 Grade (or better)				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	184	184	140	140	184	184	184
		Deflection	L/605	L/383	L/257	L/417	L/304	L/380	L/240	L/372	L/262	L/190
	20	Depth	140	140	140	184	184	140	140	184	184	235
		Deflection	L/560	L/356	L/238	L/394	L/288	L/347	L/218	L/347	L/244	L/381
	30	Depth	140	140	140	184	184	140	140	184	184	235
		Deflection	L/519	L/331	L/221	L/373	L/272	L/317	L/199	L/324	L/227	L/361
	40	Depth	140	140	140	184	184	140	184	184	235	235
		Deflection	L/482	L/308	L/205	L/353	L/257	L/289	L/444	L/302	L/463	L/342
	50	Depth	140	140	184	184	184	184	184	184	235	235
		Deflection	L/449	L/287	L/470	L/334	L/243	L/629	L/415	L/282	L/439	L/324
406	10	Depth	140	140	140	184	184	140	184	184	184	235
		Deflection	L/450	L/285	L/190	L/310	L/226	L/281	L/411	L/276	L/194	L/300
	20	Depth	140	140	184	184	184	140	184	184	235	235
		Deflection	L/413	L/261	L/413	L/291	L/211	L/253	L/379	L/255	L/385	L/282
	30	Depth	140	140	184	184	235	140	184	184	235	235
		Deflection	L/380	L/240	L/387	L/273	L/430	L/228	L/349	L/235	L/361	L/265
	40	Depth	140	184	184	184	235	184	184	235	235	286
		Deflection	L/350	L/531	L/363	L/256	L/408	L/497	L/323	L/474	L/339	L/461
	50	Depth	184	184	184	235	235	235	235	235	235	286
		Deflection	L/751	L/498	L/341	L/524	L/388	L/941	L/637	L/445	L/319	L/437
610	10	Depth	140	140	184	184	235	140	184	235	235	286
		Deflection	L/295	L/186	L/290	L/204	L/315	L/183	L/270	L/384	L/270	L/360
	20	Depth	140	184	184	235	235	184	235	235	286	286
		Deflection	L/267	L/398	L/268	L/404	L/296	L/384	L/520	L/354	L/458	L/337
	30	Depth	140	184	235	235	235	184	235	235	286	286
		Deflection	L/241	L/368	L/532	L/380	L/278	L/348	L/479	L/328	L/428	L/316
	40	Depth	184	184	235	235	286	286	286	286	286	N/A
		Deflection	L/523	L/340	L/499	L/357	L/484	L/1161	L/790	L/555	L/401	N/A
	50	Depth	235	235	235	235	286	N/A	N/A	N/A	N/A	N/A
		Deflection	L/988	L/670	L/468	L/336	L/459	N/A	N/A	N/A	N/A	N/A

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.2 (continued) - MSR Lumber Studs

Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		Grade 1650f-1.5E					Grade 2100f-1.8E				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	184	184	140	140	140	140	184
		Deflection	L/566	L/358	L/240	L/390	L/284	L/684	L/434	L/291	L/204	L/344
	20	Depth	140	140	140	184	184	140	140	140	140	184
		Deflection	L/523	L/332	L/222	L/368	L/268	L/635	L/405	L/271	L/189	L/326
	30	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/484	L/308	L/205	L/347	L/253	L/590	L/378	L/253	L/424	L/310
	40	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/449	L/286	L/189	L/328	L/239	L/550	L/353	L/236	L/402	L/294
	50	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/417	L/265	L/437	L/310	L/225	L/513	L/330	L/219	L/382	L/279
406	10	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/421	L/266	L/412	L/290	L/211	L/509	L/322	L/216	L/351	L/256
	20	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/385	L/243	L/385	L/271	L/197	L/469	L/298	L/198	L/330	L/240
	30	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/353	L/223	L/360	L/254	L/184	L/433	L/275	L/182	L/311	L/226
	40	Depth	140	140	184	184	235	140	140	184	184	184
		Deflection	L/324	L/204	L/337	L/237	L/380	L/400	L/254	L/414	L/293	L/212
	50	Depth	140	140	184	184	235	140	140	184	184	184
		Deflection	L/298	L/186	L/316	L/222	L/361	L/371	L/234	L/390	L/276	L/199
610	10	Depth	140	184	184	184	235	140	140	184	184	235
		Deflection	L/276	L/403	L/271	L/190	L/294	L/335	L/211	L/328	L/231	L/356
	20	Depth	140	184	184	235	235	140	140	184	184	235
		Deflection	L/248	L/371	L/250	L/377	L/276	L/304	L/191	L/305	L/214	L/336
	30	Depth	140	184	184	235	235	140	184	184	184	235
		Deflection	L/223	L/342	L/230	L/354	L/259	L/276	L/419	L/283	L/198	L/317
	40	Depth	184	184	184	235	235	140	184	184	184	235
		Deflection	L/487	L/316	L/212	L/332	L/243	L/251	L/389	L/263	L/184	L/299
	50	Depth	235	235	235	235	235	184	184	184	235	235
		Deflection	L/922	L/624	L/436	L/312	L/228	L/551	L/362	L/245	L/384	L/282

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.3 - Lumber Studs

Wind pressure $q_{1/50}$ 0.45 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		S-P-F No. 2 Grade (or better)					D.Fir-L No. 2 Grade (or better)				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	140	184	140	140	140	140	184
		Deflection	L/629	L/399	L/267	L/187	L/318	L/731	L/464	L/312	L/218	L/369
	20	Depth	140	140	140	184	184	140	140	140	140	184
		Deflection	L/573	L/366	L/245	L/407	L/297	L/669	L/428	L/287	L/200	L/347
	30	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/524	L/336	L/224	L/381	L/278	L/614	L/395	L/265	L/446	L/327
	40	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/481	L/308	L/204	L/357	L/260	L/566	L/365	L/244	L/420	L/307
	50	Depth	140	140	184	184	184	140	140	184	184	184
		Deflection	L/442	L/283	L/470	L/334	L/243	L/522	L/337	L/552	L/395	L/289
406	10	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/467	L/296	L/197	L/323	L/236	L/544	L/345	L/231	L/376	L/274
	20	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/422	L/267	L/425	L/300	L/218	L/494	L/314	L/209	L/350	L/255
	30	Depth	140	140	184	184	184	140	140	184	184	184
		Deflection	L/382	L/242	L/393	L/278	L/201	L/449	L/286	L/461	L/327	L/238
	40	Depth	140	140	184	184	235	140	140	184	184	235
		Deflection	L/346	L/218	L/365	L/257	L/414	L/410	L/261	L/430	L/304	L/486
	50	Depth	140	184	184	184	235	140	184	184	235	235
		Deflection	L/315	L/493	L/339	L/238	L/391	L/375	L/580	L/401	L/616	L/459
610	10	Depth	140	140	184	184	235	140	140	184	184	235
		Deflection	L/306	L/192	L/302	L/212	L/328	L/357	L/225	L/351	L/247	L/382
	20	Depth	140	184	184	184	235	140	184	184	235	235
		Deflection	L/271	L/407	L/275	L/192	L/305	L/318	L/475	L/322	L/485	L/356
	30	Depth	140	184	184	235	235	140	184	184	235	235
		Deflection	L/240	L/371	L/250	L/386	L/284	L/285	L/435	L/296	L/452	L/333
	40	Depth	184	184	235	235	235	184	184	235	235	286
		Deflection	L/517	L/338	L/500	L/359	L/264	L/607	L/399	L/586	L/422	L/573
	50	Depth	235	235	235	235	286	184	184	235	235	286
		Deflection	L/964	L/660	L/464	L/334	L/461	L/556	L/367	L/546	L/395	L/540

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.3 (continued) - Lumber Studs

Wind pressure $q_{1/50}$ 0.45 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		Hem-Fir No. 2 Grade (or better)					Northern Species No. 2 Grade (or better)				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	140	184	140	140	140	184	184
		Deflection	L/731	L/464	L/312	L/218	L/369	L/459	L/290	L/194	L/317	L/231
	20	Depth	140	140	140	140	184	140	140	184	184	184
		Deflection	L/669	L/428	L/287	L/200	L/347	L/414	L/262	L/417	L/294	L/214
	30	Depth	140	140	140	140	184	140	140	184	184	235
		Deflection	L/614	L/395	L/265	L/183	L/327	L/374	L/237	L/386	L/272	L/432
	40	Depth	140	140	140	184	184	140	184	184	184	235
		Deflection	L/566	L/365	L/244	L/420	L/307	L/339	L/522	L/358	L/252	L/406
	50	Depth	140	140	184	184	184	184	184	184	235	235
		Deflection	L/522	L/337	L/552	L/395	L/289	L/724	L/483	L/332	L/516	L/383
406	10	Depth	140	140	140	184	184	140	140	184	184	235
		Deflection	L/544	L/345	L/231	L/376	L/274	L/340	L/214	L/335	L/235	L/364
	20	Depth	140	140	140	184	184	140	140	184	184	235
		Deflection	L/494	L/314	L/209	L/350	L/255	L/302	L/190	L/306	L/215	L/339
	30	Depth	140	140	184	184	184	140	184	184	235	235
		Deflection	L/449	L/286	L/461	L/327	L/238	L/270	L/414	L/280	L/430	L/317
	40	Depth	140	140	184	184	235	184	184	184	235	235
		Deflection	L/410	L/261	L/430	L/304	L/486	L/577	L/379	L/257	L/401	L/296
	50	Depth	184	184	184	184	235	235	235	235	235	286
		Deflection	L/865	L/580	L/401	L/284	L/459	L/1071	L/735	L/519	L/375	L/514
610	10	Depth	140	140	184	184	235	140	184	184	235	235
		Deflection	L/357	L/225	L/351	L/247	L/382	L/221	L/326	L/219	L/328	L/239
	20	Depth	140	140	184	184	235	184	184	235	235	286
		Deflection	L/318	L/200	L/322	L/226	L/356	L/456	L/293	L/424	L/301	L/405
	30	Depth	140	184	184	235	235	184	235	235	286	286
		Deflection	L/285	L/435	L/296	L/452	L/333	L/408	L/563	L/389	L/508	L/377
	40	Depth	184	184	235	235	235	286	286	286	286	286
		Deflection	L/607	L/399	L/586	L/422	L/311	L/1323	L/912	L/648	L/472	L/351
	50	Depth	235	235	235	235	286	N/A	N/A	N/A	N/A	N/A
		Deflection	L/1125	L/773	L/546	L/395	L/540	N/A	N/A	N/A	N/A	N/A

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.3 (continued) - MSR Lumber Studs

Wind pressure $q_{1/50}$ 0.45 kPa

Depth required (mm) for 38 mm thick studs

Stud spacing mm	Factored axial load kN/m		Grade 1650f-1.5E					Grade 2100f-1.8E				
			Stud length					Stud length				
			3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)	3.66 m (12 ft)	4.27 m (14 ft)	4.88 m (16 ft)	5.49 m (18 ft)	6.10 m (20 ft)
305	10	Depth	140	140	140	140	184	89	140	140	140	184
		Deflection	L/683	L/434	L/291	L/204	L/345	L/204	L/525	L/353	L/248	L/418
	20	Depth	140	140	140	140	184	140	140	140	140	184
		Deflection	L/624	L/399	L/268	L/186	L/324	L/758	L/486	L/327	L/229	L/394
	30	Depth	140	140	140	184	184	140	140	140	140	184
		Deflection	L/572	L/367	L/246	L/416	L/304	L/698	L/451	L/303	L/211	L/372
	40	Depth	140	140	140	184	184	140	140	140	140	184
		Deflection	L/526	L/338	L/225	L/390	L/285	L/645	L/418	L/281	L/194	L/351
	50	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/485	L/312	L/206	L/367	L/268	L/597	L/388	L/260	L/452	L/332
406	10	Depth	140	140	140	184	184	140	140	140	140	184
		Deflection	L/508	L/322	L/215	L/352	L/256	L/615	L/390	L/262	L/183	L/311
	20	Depth	140	140	140	184	184	140	140	140	184	184
		Deflection	L/460	L/292	L/194	L/327	L/238	L/560	L/358	L/239	L/398	L/291
	30	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/418	L/265	L/429	L/304	L/221	L/512	L/328	L/218	L/372	L/272
	40	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/380	L/241	L/399	L/282	L/204	L/469	L/301	L/199	L/348	L/254
	50	Depth	140	140	184	184	184	140	140	140	184	184
		Deflection	L/347	L/218	L/372	L/263	L/189	L/431	L/276	L/181	L/326	L/237
610	10	Depth	140	140	184	184	235	140	140	184	184	184
		Deflection	L/333	L/210	L/328	L/230	L/357	L/404	L/255	L/398	L/280	L/204
	20	Depth	140	140	184	184	235	140	140	184	184	184
		Deflection	L/296	L/185	L/300	L/210	L/332	L/363	L/229	L/366	L/258	L/187
	30	Depth	140	184	184	184	235	140	140	184	184	235
		Deflection	L/264	L/405	L/274	L/192	L/310	L/326	L/205	L/338	L/237	L/379
	40	Depth	184	184	184	235	235	140	140	184	184	235
		Deflection	L/565	L/371	L/251	L/393	L/289	L/294	L/183	L/312	L/218	L/356
	50	Depth	235	235	235	235	235	184	184	184	184	235
		Deflection	L/1050	L/720	L/508	L/367	L/270	L/634	L/421	L/288	L/201	L/334

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions.
- The Canadian Wood Council recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended.
- All sizes may not be available in both grades. Before specifying, the designer should ensure that the studs are available in the size, length and grade specified. Stud tables for additional lengths are available at www.wood-works.org.
- Nominal imperial equivalents for the stud depths are:

depth mm	140	184	235	286
nominal depth inches	6	8	10	12

Table 2.4 - VERSA-STUD® 2400 by BOISE



Wind pressure $q_{1/50} = 0.65 \text{ kPa}$

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		VERSA-LAM® 2400 1.7 E									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/459	L/236	L/323	L/203	L/290	L/203	L/271	L/203	L/184	L/240
	20	Depth	140	140	184	184	235	235	286	286	356	356
		Deflection	L/401	L/205	L/292	L/182	L/267	L/187	L/253	L/189	L/290	L/228
	30	Depth	140	184	184	235	235	241	286	302	356	356
		Deflection	L/352	L/450	L/264	L/368	L/247	L/187	L/237	L/211	L/275	L/216
	40	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/310	L/407	L/239	L/340	L/228	L/305	L/222	L/198	L/261	L/204
	50	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/273	L/370	L/215	L/315	L/210	L/286	L/207	L/185	L/248	L/193
406	10	Depth	140	184	184	235	235	286	286	356	356	406
		Deflection	L/339	L/412	L/239	L/321	L/215	L/276	L/201	L/296	L/228	L/270
	20	Depth	140	184	184	235	235	286	286	356	356	406
		Deflection	L/291	L/366	L/212	L/293	L/195	L/256	L/186	L/278	L/214	L/256
	30	Depth	140	184	184	235	241	286	302	356	356	406
		Deflection	L/250	L/326	L/188	L/267	L/194	L/237	L/205	L/262	L/201	L/242
	40	Depth	140	184	235	235	286	286	302	356	356	406
		Deflection	L/215	L/291	L/383	L/244	L/313	L/220	L/191	L/247	L/189	L/230
	50	Depth	140	184	235	235	286	286	356	356	406	406
		Deflection	L/185	L/261	L/350	L/223	L/291	L/204	L/309	L/232	L/277	L/218
610	10	Depth	140	184	235	235	286	286	356	356	406	--
		Deflection	L/218	L/268	L/332	L/209	L/257	L/180	L/258	L/194	L/225	N/A
	20	Depth	184	184	235	235	286	302	356	406	406	--
		Deflection	L/443	L/232	L/296	L/186	L/234	L/195	L/240	L/274	L/211	N/A
	30	Depth	184	184	235	241	286	356	356	406	406	--
		Deflection	L/384	L/201	L/265	L/182	L/214	L/305	L/223	L/257	L/197	N/A
	40	Depth	184	235	235	286	286	356	356	406	406	--
		Deflection	L/335	L/398	L/238	L/290	L/195	L/283	L/207	L/241	L/185	N/A
	50	Depth	184	235	235	286	302	356	356	406	--	--
		Deflection	L/294	L/358	L/213	L/265	L/215	L/263	L/192	L/226	N/A	N/A

Notes:

- THIS TABLE IS FOR PRELIMINARY SIZING ONLY. The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Boise at 1-800-964-6999. Other sizes and grades are available.
- BOISE recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m. The blocking must meet the shearwall requirements for the application.
- Sizes shown in the table are based on Dry Service conditions.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	241	286	302	356	406
depth inches	5-1/2	7-1/4	9-1/4	9-1/2	11-1/4	11-7/8	14	16

Table 2.4 (continued) - VERSA-STUD® 2800 by BOISE



Wind pressure $q_{1/50} = 0.65$ kPa

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		VERSA-LAM® 2800 2.0 E									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	184	184	235	235	241	286	286	356
		Deflection	L/544	L/281	L/383	L/241	L/343	L/241	L/190	L/240	L/185	L/284
	20	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/479	L/248	L/349	L/219	L/319	L/223	L/301	L/226	L/206	L/271
	30	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/424	L/218	L/318	L/198	L/296	L/207	L/284	L/212	L/193	L/258
	40	Depth	140	140	184	235	235	235	286	286	302	356
		Deflection	L/377	L/192	L/290	L/408	L/275	L/191	L/267	L/199	L/182	L/245
	50	Depth	140	184	184	235	235	241	286	286	356	356
		Deflection	L/336	L/448	L/265	L/380	L/256	L/194	L/251	L/186	L/298	L/233
406	10	Depth	140	140	184	235	235	241	286	302	356	356
		Deflection	L/403	L/206	L/284	L/380	L/255	L/194	L/238	L/211	L/269	L/212
	20	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/350	L/436	L/255	L/349	L/234	L/305	L/222	L/197	L/255	L/200
	30	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/304	L/392	L/229	L/321	L/214	L/284	L/206	L/184	L/241	L/188
	40	Depth	140	184	184	235	235	286	286	356	356	406
		Deflection	L/266	L/353	L/205	L/295	L/196	L/265	L/192	L/296	L/227	L/275
	50	Depth	140	184	184	235	241	286	302	356	356	406
		Deflection	L/232	L/319	L/183	L/272	L/198	L/248	L/215	L/280	L/215	L/262
610	10	Depth	140	184	184	235	241	286	302	356	406	406
		Deflection	L/261	L/318	L/184	L/248	L/180	L/214	L/184	L/230	L/266	L/209
	20	Depth	140	184	235	235	286	286	356	356	406	406
		Deflection	L/219	L/279	L/354	L/224	L/280	L/196	L/286	L/214	L/251	L/197
	30	Depth	140	184	235	235	286	302	356	356	406	406
		Deflection	L/184	L/245	L/319	L/201	L/257	L/215	L/267	L/200	L/236	L/185
	40	Depth	184	184	235	235	286	302	356	356	406	--
		Deflection	L/406	L/215	L/289	L/181	L/236	L/198	L/249	L/186	L/222	N/A
	50	Depth	184	184	235	286	286	302	356	406	406	--
		Deflection	L/359	L/189	L/261	L/322	L/217	L/182	L/233	L/272	L/209	N/A

Notes:

- THIS TABLE IS FOR PRELIMINARY SIZING ONLY. The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Boise at 1-800-964-6999. Other sizes and grades are available.
- BOISE recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m. The blocking must meet the shearwall requirements for the application.
- Sizes shown in the table are based on Dry Service conditions.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	241	286	302	356	406
depth inches	5-1/2	7-1/4	9-1/4	9-1/2	11-1/4	11-7/8	14	16

Table 2.5 - VERSA-STUD® 2400 by BOISE



Wind pressure $q_{1/50} = 0.55 \text{ kPa}$

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		VERSA-LAM® 2400 1.7 E									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	184	184	235	235	241	286	286	356
		Deflection	L/534	L/276	L/379	L/238	L/340	L/238	L/188	L/239	L/183	L/283
	20	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/460	L/238	L/339	L/212	L/312	L/218	L/296	L/222	L/202	L/267
	30	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/400	L/205	L/304	L/189	L/286	L/199	L/276	L/206	L/188	L/252
	40	Depth	140	184	184	235	235	235	286	286	356	356
		Deflection	L/348	L/461	L/273	L/390	L/262	L/181	L/257	L/191	L/303	L/238
	50	Depth	140	184	184	235	235	241	286	302	356	356
		Deflection	L/305	L/415	L/245	L/358	L/241	L/182	L/239	L/214	L/286	L/224
406	10	Depth	140	140	184	235	235	241	286	302	356	356
		Deflection	L/394	L/202	L/280	L/376	L/252	L/192	L/236	L/209	L/268	L/210
	20	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/334	L/422	L/246	L/340	L/228	L/299	L/217	L/193	L/251	L/196
	30	Depth	140	184	184	235	235	286	286	356	356	356
		Deflection	L/284	L/372	L/216	L/308	L/205	L/275	L/199	L/305	L/234	L/183
	40	Depth	140	184	184	235	235	286	286	356	356	406
		Deflection	L/242	L/330	L/190	L/279	L/185	L/254	L/183	L/285	L/219	L/267
	50	Depth	140	184	235	235	241	286	302	356	356	406
		Deflection	L/206	L/292	L/395	L/253	L/184	L/234	L/204	L/267	L/205	L/252
610	10	Depth	140	184	184	235	286	286	302	356	406	406
		Deflection	L/254	L/312	L/180	L/245	L/301	L/212	L/182	L/228	L/265	L/208
	20	Depth	140	184	235	235	286	286	356	356	406	406
		Deflection	L/207	L/268	L/342	L/216	L/273	L/191	L/280	L/210	L/247	L/194
	30	Depth	184	184	235	235	286	302	356	356	406	406
		Deflection	L/432	L/230	L/304	L/191	L/247	L/207	L/258	L/193	L/230	L/180
	40	Depth	184	184	235	241	286	302	356	406	406	--
		Deflection	L/373	L/197	L/270	L/186	L/223	L/187	L/238	L/278	L/214	N/A
	50	Depth	184	235	235	286	286	356	356	406	406	--
		Deflection	L/325	L/399	L/240	L/300	L/202	L/301	L/220	L/259	L/199	N/A

Notes:

1. THIS TABLE IS FOR PRELIMINARY SIZING ONLY. The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Boise at 1-800-964-6999. Other sizes and grades are available.
2. BOISE recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
4. Maximum spacing of full depth blocking is 2.4 m. The blocking must meet the shearwall requirements for the application.
5. Sizes shown in the table are based on Dry Service conditions.
6. Imperial equivalents for the stud depths are:

depth mm	140	184	235	241	286	302	356	406
depth inches	5-1/2	7-1/4	9-1/4	9-1/2	11-1/4	11-7/8	14	16

Table 2.5 (continued) - VERSA-STUD® 2800 by BOISE



Wind pressure $q_{1/50} = 0.55$ kPa

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		VERSA-LAM® 2800 2.0 E									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	286	286	302
		Deflection	L/632	L/328	L/188	L/283	L/188	L/283	L/205	L/283	L/217	L/201
	20	Depth	140	140	184	184	235	235	235	286	286	302
		Deflection	L/550	L/287	L/405	L/255	L/372	L/261	L/189	L/264	L/203	L/188
	30	Depth	140	140	184	184	235	235	241	286	286	356
		Deflection	L/482	L/251	L/366	L/230	L/343	L/240	L/189	L/247	L/189	L/301
	40	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/424	L/219	L/332	L/207	L/317	L/221	L/309	L/231	L/212	L/285
	50	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/375	L/190	L/301	L/185	L/293	L/203	L/290	L/216	L/198	L/271
406	10	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/469	L/241	L/332	L/209	L/299	L/209	L/280	L/210	L/191	L/249
	20	Depth	140	140	184	184	235	235	286	286	356	356
		Deflection	L/401	L/206	L/296	L/184	L/273	L/190	L/259	L/194	L/298	L/234
	30	Depth	140	184	184	235	235	241	286	302	356	356
		Deflection	L/346	L/447	L/263	L/370	L/248	L/189	L/240	L/214	L/280	L/220
	40	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/299	L/400	L/234	L/338	L/226	L/306	L/222	L/199	L/264	L/206
	50	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/259	L/358	L/208	L/309	L/206	L/284	L/205	L/184	L/248	L/194
610	10	Depth	140	184	184	235	235	286	286	356	356	406
		Deflection	L/303	L/371	L/215	L/291	L/194	L/251	L/182	L/270	L/208	L/246
	20	Depth	140	184	184	235	241	286	302	356	356	406
		Deflection	L/251	L/322	L/185	L/260	L/189	L/229	L/197	L/251	L/192	L/231
	30	Depth	140	184	235	235	286	286	302	356	406	406
		Deflection	L/208	L/280	L/365	L/232	L/297	L/208	L/180	L/232	L/275	L/216
	40	Depth	184	184	235	235	286	286	356	356	406	406
		Deflection	L/452	L/244	L/328	L/207	L/271	L/189	L/287	L/216	L/258	L/202
	50	Depth	184	184	235	235	286	302	356	356	406	406
		Deflection	L/397	L/212	L/295	L/185	L/248	L/209	L/267	L/200	L/242	L/189

Notes:

1. THIS TABLE IS FOR PRELIMINARY SIZING ONLY. The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Boise at 1-800-964-6999. Other sizes and grades are available.
2. BOISE recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
4. Maximum spacing of full depth blocking is 2.4 m. The blocking must meet the shearwall requirements for the application.
5. Sizes shown in the table are based on Dry Service conditions.
6. Imperial equivalents for the stud depths are:

depth mm	140	184	235	241	286	302	356	406
depth inches	5-1/2	7-1/4	9-1/4	9-1/2	11-1/4	11-7/8	14	16

Table 2.6 - VERSA-STUD® 2400 by BOISE



Wind pressure $q_{1/50} = 0.45$ kPa

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		VERSA-LAM® 2400 1.7 E									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	286	286	302
		Deflection	L/638	L/332	L/190	L/288	L/192	L/289	L/210	L/290	L/223	L/207
	20	Depth	140	140	184	184	235	235	235	286	286	302
		Deflection	L/540	L/283	L/404	L/255	L/374	L/262	L/189	L/268	L/205	L/191
	30	Depth	140	140	184	184	235	235	241	286	286	356
		Deflection	L/462	L/241	L/358	L/224	L/340	L/238	L/187	L/247	L/188	L/303
	40	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/398	L/204	L/319	L/197	L/310	L/215	L/305	L/228	L/209	L/284
	50	Depth	140	184	184	235	235	235	286	286	302	356
		Deflection	L/345	L/473	L/283	L/416	L/282	L/194	L/282	L/210	L/193	L/267
406	10	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/471	L/243	L/337	L/212	L/305	L/213	L/286	L/215	L/195	L/256
	20	Depth	140	140	184	184	235	235	286	286	356	356
		Deflection	L/392	L/201	L/293	L/182	L/273	L/190	L/261	L/195	L/302	L/237
	30	Depth	140	184	184	235	235	241	286	302	356	356
		Deflection	L/329	L/433	L/255	L/364	L/244	L/185	L/238	L/213	L/281	L/220
	40	Depth	140	184	184	235	235	286	286	302	356	356
		Deflection	L/276	L/379	L/222	L/327	L/218	L/300	L/217	L/194	L/261	L/204
	50	Depth	140	184	184	235	235	286	286	356	356	356
		Deflection	L/233	L/333	L/192	L/294	L/195	L/274	L/198	L/316	L/243	L/189
610	10	Depth	140	184	184	235	235	286	286	356	356	406
		Deflection	L/303	L/374	L/217	L/295	L/197	L/256	L/186	L/276	L/213	L/253
	20	Depth	140	184	184	235	241	286	302	356	356	406
		Deflection	L/242	L/316	L/182	L/258	L/187	L/229	L/198	L/253	L/194	L/234
	30	Depth	140	184	235	235	286	286	356	356	406	406
		Deflection	L/194	L/267	L/355	L/226	L/292	L/204	L/307	L/231	L/275	L/216
	40	Depth	184	184	235	235	286	286	356	356	406	406
		Deflection	L/421	L/227	L/312	L/197	L/262	L/182	L/282	L/211	L/254	L/199
	50	Depth	184	184	235	241	286	302	356	356	406	406
		Deflection	L/362	L/192	L/275	L/190	L/235	L/199	L/258	L/193	L/235	L/183

Notes:

1. THIS TABLE IS FOR PRELIMINARY SIZING ONLY. The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Boise at 1-800-964-6999. Other sizes and grades are available.
2. BOISE recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
4. Maximum spacing of full depth blocking is 2.4 m. The blocking must meet the shearwall requirements for the application.
5. Sizes shown in the table are based on Dry Service conditions.
6. Imperial equivalents for the stud depths are:

depth mm	140	184	235	241	286	302	356	406
depth inches	5-1/2	7-1/4	9-1/4	9-1/2	11-1/4	11-7/8	14	16

Table 2.6 (continued) - **VERSA-STUD® 2800** by **BOISE**



Wind pressure $q_{1/50} = 0.45$ kPa

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		VERSA-LAM® 2800 2.0 E									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/756	L/395	L/228	L/342	L/228	L/343	L/249	L/186	L/264	L/207
	20	Depth	140	140	140	184	184	235	235	241	286	286
		Deflection	L/646	L/341	L/194	L/306	L/203	L/314	L/228	L/185	L/245	L/191
	30	Depth	140	140	184	184	235	235	235	286	286	302
		Deflection	L/557	L/295	L/432	L/273	L/408	L/287	L/207	L/297	L/227	L/212
	40	Depth	140	140	184	184	235	235	235	286	286	302
		Deflection	L/485	L/255	L/387	L/244	L/374	L/263	L/188	L/276	L/210	L/197
	50	Depth	140	140	184	184	235	235	241	286	286	302
		Deflection	L/424	L/219	L/348	L/217	L/344	L/240	L/188	L/256	L/194	L/182
406	10	Depth	140	140	184	184	235	235	235	286	286	302
		Deflection	L/560	L/291	L/401	L/252	L/362	L/254	L/184	L/255	L/195	L/181
	20	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/471	L/244	L/352	L/221	L/327	L/229	L/312	L/234	L/213	L/283
	30	Depth	140	140	184	184	235	235	286	286	302	356
		Deflection	L/400	L/205	L/310	L/192	L/295	L/205	L/287	L/214	L/196	L/264
	40	Depth	140	184	184	235	235	235	286	286	356	356
		Deflection	L/341	L/460	L/273	L/396	L/267	L/184	L/264	L/196	L/315	L/247
	50	Depth	140	184	184	235	235	241	286	302	356	356
		Deflection	L/292	L/408	L/241	L/359	L/241	L/182	L/243	L/218	L/294	L/230
610	10	Depth	140	140	184	235	235	286	286	302	356	356
		Deflection	L/362	L/185	L/259	L/351	L/235	L/304	L/221	L/196	L/252	L/198
	20	Depth	140	184	184	235	235	286	286	356	356	356
		Deflection	L/295	L/380	L/221	L/310	L/207	L/274	L/199	L/301	L/232	L/181
	30	Depth	140	184	184	235	235	286	302	356	356	406
		Deflection	L/241	L/326	L/187	L/274	L/181	L/248	L/215	L/278	L/213	L/259
	40	Depth	140	184	235	235	286	286	302	356	356	406
		Deflection	L/197	L/280	L/379	L/243	L/318	L/223	L/195	L/256	L/196	L/241
	50	Depth	184	184	235	235	286	286	356	356	406	406
		Deflection	L/443	L/242	L/338	L/214	L/288	L/201	L/313	L/236	L/285	L/224

Notes:

1. THIS TABLE IS FOR PRELIMINARY SIZING ONLY. The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Boise at 1-800-964-6999. Other sizes and grades are available.
2. BOISE recommends that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker waferboard, plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
4. Maximum spacing of full depth blocking is 2.4 m. The blocking must meet the shearwall requirements for the application.
5. Sizes shown in the table are based on Dry Service conditions.
6. Imperial equivalents for the stud depths are:

depth mm	140	184	235	241	286	302	356	406
depth inches	5-1/2	7-1/4	9-1/4	9-1/2	11-1/4	11-7/8	14	16

Table 2.7 - LP LVL Studs - Louisiana-Pacific

Wind pressure $q_{1/50}$ 0.65 kPa



Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		2250Fb-1.5E LP LVL									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/482	L/247	L/334	L/210	L/296	L/208	L/275	L/206	L/261	L/205
	20	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/447	L/230	L/316	L/198	L/284	L/199	L/265	L/199	L/253	L/199
	30	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/416	L/214	L/299	L/187	L/272	L/190	L/256	L/192	L/246	L/193
	40	Depth	140	140	184	235	235	235	286	286	337	337
		Deflection	L/388	L/198	L/284	L/388	L/260	L/181	L/247	L/185	L/239	L/187
	50	Depth	140	140	184	235	235	286	286	337	337	337
		Deflection	L/361	L/184	L/269	L/371	L/249	L/327	L/238	L/301	L/231	L/181
406	10	Depth	140	140	184	235	235	286	286	337	337	N/A
		Deflection	L/358	L/183	L/248	L/329	L/220	L/281	L/205	L/253	L/195	N/A
	20	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/330	L/401	L/233	L/313	L/210	L/270	L/196	L/244	L/188	N/A
	30	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/304	L/377	L/219	L/298	L/199	L/259	L/188	L/236	L/181	N/A
	40	Depth	140	184	184	235	235	286	286	337	N/A	N/A
		Deflection	L/280	L/354	L/205	L/284	L/189	L/249	L/180	L/228	N/A	N/A
	50	Depth	140	184	184	235	286	286	337	337	N/A	N/A
		Deflection	L/258	L/333	L/192	L/270	L/340	L/239	L/293	L/220	N/A	N/A
610	10	Depth	140	184	235	235	286	286	337	N/A	N/A	N/A
		Deflection	L/235	L/282	L/344	L/217	L/264	L/186	L/223	N/A	N/A	N/A
	20	Depth	140	184	235	235	286	337	337	N/A	N/A	N/A
		Deflection	L/212	L/261	L/324	L/204	L/252	L/293	L/214	N/A	N/A	N/A
	30	Depth	140	184	235	235	286	337	337	N/A	N/A	N/A
		Deflection	L/191	L/242	L/305	L/192	L/239	L/281	L/205	N/A	N/A	N/A
	40	Depth	184	184	235	235	286	337	337	N/A	N/A	N/A
		Deflection	L/427	L/224	L/287	L/180	L/228	L/269	L/196	N/A	N/A	N/A
	50	Depth	184	184	235	286	286	337	337	N/A	N/A	N/A
		Deflection	L/396	L/207	L/271	L/322	L/217	L/258	L/188	N/A	N/A	N/A

Notes:

- The designer must assure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact LP at 1-888-820-0325.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with minimum 9.5mm thick plywood or OSB and fastened to meet the requirements of the National Building Code of Canada, unless greater requirements are specified by the project engineer. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada.
- Full depth blocking is required at 2.4 m on centre, unless greater requirements are specified by the project engineer.
- The wall plates are assumed to be of the same material as the studs. The resistance of the wall plates must be checked in accordance with CSA O86.
- The connection between the studs and the wall plates must be designed by the project engineer.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	337
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/4

Table 2.7 (continued) - LP LVL Studs - Louisiana-Pacific



BUILDING PRODUCTS

Wind pressure $q_{1/50}$ 0.65 kPa

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		2950Fb-2.0E LP LVL									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	286	286	337
		Deflection	L/646	L/333	L/192	L/282	L/189	L/279	L/203	L/276	L/213	L/275
	20	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/605	L/313	L/427	L/269	L/382	L/269	L/195	L/268	L/206	L/268
	30	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/566	L/294	L/407	L/257	L/368	L/259	L/187	L/260	L/200	L/261
	40	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/531	L/276	L/389	L/245	L/355	L/249	L/180	L/252	L/193	L/254
	50	Depth	140	140	184	184	235	235	286	286	286	337
		Deflection	L/499	L/260	L/371	L/233	L/342	L/240	L/326	L/244	L/187	L/248
406	10	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/482	L/247	L/334	L/210	L/296	L/208	L/275	L/206	L/261	L/205
	20	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/447	L/230	L/316	L/198	L/284	L/199	L/265	L/199	L/253	L/199
	30	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/416	L/214	L/299	L/187	L/272	L/190	L/256	L/192	L/246	L/193
	40	Depth	140	140	184	235	235	235	286	286	337	337
		Deflection	L/388	L/198	L/284	L/388	L/260	L/181	L/247	L/185	L/239	L/187
	50	Depth	140	140	184	235	235	286	286	337	337	337
		Deflection	L/361	L/184	L/269	L/371	L/249	L/327	L/238	L/301	L/231	L/181
610	10	Depth	140	184	184	235	235	286	286	337	N/A	N/A
		Deflection	L/317	L/379	L/220	L/292	L/195	L/249	L/181	L/224	N/A	N/A
	20	Depth	140	184	184	235	235	286	337	337	N/A	N/A
		Deflection	L/290	L/355	L/205	L/277	L/185	L/239	L/288	L/216	N/A	N/A
	30	Depth	140	184	184	235	286	286	337	337	N/A	N/A
		Deflection	L/266	L/332	L/192	L/263	L/325	L/229	L/278	L/208	N/A	N/A
	40	Depth	140	184	235	235	286	286	337	337	N/A	N/A
		Deflection	L/244	L/311	L/393	L/249	L/312	L/219	L/268	L/201	N/A	N/A
	50	Depth	140	184	235	235	286	286	337	337	N/A	N/A
		Deflection	L/224	L/291	L/373	L/237	L/299	L/209	L/258	L/193	N/A	N/A

Notes:

- The designer must assure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact LP at 1-888-820-0325.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with minimum 9.5mm thick plywood or OSB and fastened to meet the requirements of the National Building Code of Canada, unless greater requirements are specified by the project engineer. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada.
- Full depth blocking is required at 2.4 m on centre, unless greater requirements are specified by the project engineer.
- The wall plates are assumed to be of the same material as the studs. The resistance of the wall plates must be checked in accordance with CSA O86.
- The connection between the studs and the wall plates must be designed by the project engineer.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	337
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/4

Table 2.8 - LP LVL Studs - Louisiana-Pacific

Wind pressure $q_{1/50}$ 0.55 kPa



Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		2250Fb-1.5E LP LVL									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	184	184	235	235	286	286	286	337
		Deflection	L/564	L/291	L/392	L/247	L/349	L/245	L/324	L/243	L/187	L/242
	20	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/520	L/269	L/370	L/233	L/333	L/233	L/312	L/234	L/298	L/234
	30	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/480	L/248	L/349	L/219	L/318	L/222	L/300	L/225	L/288	L/226
	40	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/444	L/229	L/329	L/206	L/303	L/212	L/289	L/216	L/279	L/219
	50	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/412	L/211	L/310	L/193	L/290	L/202	L/278	L/208	L/270	L/212
406	10	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/420	L/215	L/292	L/183	L/260	L/182	L/241	L/181	L/230	L/180
	20	Depth	140	140	184	235	235	286	286	337	337	N/A
		Deflection	L/383	L/196	L/273	L/367	L/246	L/317	L/231	L/287	L/221	N/A
	30	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/350	L/436	L/254	L/348	L/233	L/303	L/221	L/277	L/213	N/A
	40	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/321	L/407	L/238	L/330	L/220	L/290	L/211	L/267	L/205	N/A
	50	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/294	L/381	L/222	L/313	L/209	L/278	L/201	L/257	L/197	N/A
610	10	Depth	140	184	184	235	286	286	337	337	N/A	N/A
		Deflection	L/275	L/331	L/191	L/255	L/311	L/218	L/262	L/197	N/A	N/A
	20	Depth	140	184	235	235	286	286	337	337	N/A	N/A
		Deflection	L/246	L/304	L/378	L/239	L/295	L/207	L/251	L/188	N/A	N/A
	30	Depth	140	184	235	235	286	286	337	N/A	N/A	N/A
		Deflection	L/221	L/280	L/354	L/224	L/279	L/196	L/239	N/A	N/A	N/A
	40	Depth	140	184	235	235	286	286	337	N/A	N/A	N/A
		Deflection	L/197	L/258	L/331	L/209	L/265	L/185	L/229	N/A	N/A	N/A
	50	Depth	184	184	235	235	286	337	337	N/A	N/A	N/A
		Deflection	L/447	L/237	L/311	L/196	L/251	L/299	L/218	N/A	N/A	N/A

Notes:

- The designer must assure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact LP at 1-888-820-0325.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with minimum 9.5mm thick plywood or OSB and fastened to meet the requirements of the National Building Code of Canada, unless greater requirements are specified by the project engineer. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada.
- Full depth blocking is required at 2.4 m on centre, unless greater requirements are specified by the project engineer.
- The wall plates are assumed to be of the same material as the studs. The resistance of the wall plates must be checked in accordance with CSA O86.
- The connection between the studs and the wall plates must be designed by the project engineer.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	337
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/4

Table 2.8 (continued) - LP LVL Studs - Louisiana-Pacific



BUILDING PRODUCTS

Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		2950Fb-2.0E LP LVL									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/757	L/392	L/226	L/332	L/222	L/328	L/239	L/326	L/251	L/197
	20	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/703	L/366	L/211	L/316	L/211	L/315	L/229	L/315	L/243	L/190
	30	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/653	L/342	L/196	L/300	L/199	L/303	L/220	L/305	L/234	L/183
	40	Depth	140	140	140	184	184	235	235	286	286	337
		Deflection	L/609	L/320	L/182	L/285	L/188	L/291	L/211	L/295	L/226	L/298
	50	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/569	L/299	L/428	L/270	L/397	L/279	L/202	L/285	L/219	L/290
406	10	Depth	140	140	184	184	235	235	286	286	286	337
		Deflection	L/564	L/291	L/392	L/247	L/349	L/245	L/324	L/243	L/187	L/242
	20	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/520	L/269	L/370	L/233	L/333	L/233	L/312	L/234	L/298	L/234
	30	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/480	L/248	L/349	L/219	L/318	L/222	L/300	L/225	L/288	L/226
	40	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/444	L/229	L/329	L/206	L/303	L/212	L/289	L/216	L/279	L/219
	50	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/412	L/211	L/310	L/193	L/290	L/202	L/278	L/208	L/270	L/212
610	10	Depth	140	140	184	235	235	286	286	337	337	N/A
		Deflection	L/371	L/190	L/258	L/343	L/230	L/293	L/214	L/264	L/204	N/A
	20	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/337	L/413	L/240	L/324	L/217	L/280	L/204	L/254	L/195	N/A
	30	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/307	L/384	L/223	L/306	L/205	L/267	L/194	L/244	L/187	N/A
	40	Depth	140	184	184	235	235	286	286	337	N/A	N/A
		Deflection	L/280	L/357	L/207	L/289	L/193	L/255	L/185	L/235	N/A	N/A
	50	Depth	140	184	184	235	235	286	337	337	N/A	N/A
		Deflection	L/255	L/333	L/192	L/274	L/182	L/243	L/300	L/225	N/A	N/A

Notes:

- The designer must assure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact LP at 1-888-820-0325.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with minimum 9.5mm thick plywood or OSB and fastened to meet the requirements of the National Building Code of Canada, unless greater requirements are specified by the project engineer. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada.
- Full depth blocking is required at 2.4 m on centre, unless greater requirements are specified by the project engineer.
- The wall plates are assumed to be of the same material as the studs. The resistance of the wall plates must be checked in accordance with CSA O86.
- The connection between the studs and the wall plates must be designed by the project engineer.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	337
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/4

Table 2.9 - LP LVL Studs - Louisiana-Pacific

Wind pressure $q_{1/50}$ 0.45 kPa



Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		2250Fb-1.5E LP LVL									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	286	286	337
		Deflection	L/681	L/352	L/203	L/300	L/201	L/298	L/217	L/296	L/228	L/295
	20	Depth	140	140	140	184	184	235	235	286	286	337
		Deflection	L/621	L/323	L/185	L/281	L/187	L/283	L/205	L/284	L/218	L/284
	30	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/568	L/297	L/417	L/263	L/382	L/268	L/194	L/272	L/208	L/274
	40	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/520	L/272	L/391	L/246	L/363	L/255	L/184	L/260	L/199	L/265
	50	Depth	140	140	184	184	235	235	286	286	286	337
		Deflection	L/479	L/249	L/367	L/230	L/345	L/242	L/333	L/249	L/190	L/255
406	10	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/506	L/261	L/354	L/223	L/315	L/221	L/294	L/220	L/280	L/220
	20	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/457	L/236	L/328	L/206	L/297	L/208	L/280	L/209	L/268	L/211
	30	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/414	L/213	L/305	L/190	L/280	L/195	L/266	L/199	L/257	L/202
	40	Depth	140	140	184	235	235	235	286	286	337	337
		Deflection	L/376	L/191	L/283	L/392	L/264	L/183	L/253	L/189	L/247	L/193
	50	Depth	140	184	184	235	235	286	286	337	337	337
		Deflection	L/342	L/445	L/262	L/370	L/249	L/331	L/241	L/308	L/237	L/185
610	10	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/332	L/400	L/232	L/310	L/207	L/266	L/193	L/240	L/184	N/A
	20	Depth	140	184	184	235	235	286	286	337	N/A	N/A
		Deflection	L/294	L/364	L/211	L/288	L/192	L/250	L/182	L/228	N/A	N/A
	30	Depth	140	184	184	235	286	286	337	337	N/A	N/A
		Deflection	L/261	L/332	L/192	L/268	L/335	L/236	L/288	L/216	N/A	N/A
	40	Depth	140	184	235	235	286	286	337	337	N/A	N/A
		Deflection	L/231	L/304	L/392	L/249	L/316	L/222	L/274	L/205	N/A	N/A
	50	Depth	184	184	235	235	286	286	337	337	N/A	N/A
		Deflection	L/514	L/278	L/365	L/232	L/298	L/209	L/261	L/195	N/A	N/A

Notes:

- The designer must assure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact LP at 1-888-820-0325.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with minimum 9.5mm thick plywood or OSB and fastened to meet the requirements of the National Building Code of Canada, unless greater requirements are specified by the project engineer. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada.
- Full depth blocking is required at 2.4 m on centre, unless greater requirements are specified by the project engineer.
- The wall plates are assumed to be of the same material as the studs. The resistance of the wall plates must be checked in accordance with CSA O86.
- The connection between the studs and the wall plates must be designed by the project engineer.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	337
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/4

Table 2.9 (continued) - LP LVL Studs - Louisiana-Pacific



BUILDING PRODUCTS

Wind pressure $q_{1/50}$ 0.45 kPa

Depth required (mm) for 38 mm (1-1/2") thick studs

Stud spacing mm	Factored axial load kN/m		2950Fb-2.0E LP LVL									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	184	235	235	286	286
		Deflection	L/914	L/475	L/275	L/404	L/270	L/189	L/291	L/218	L/306	L/240
	20	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/838	L/440	L/255	L/382	L/255	L/382	L/278	L/208	L/295	L/231
	30	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/772	L/409	L/235	L/361	L/241	L/366	L/266	L/198	L/284	L/222
	40	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/713	L/380	L/217	L/341	L/227	L/350	L/254	L/189	L/274	L/214
	50	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/661	L/353	L/200	L/322	L/213	L/335	L/243	L/343	L/263	L/206
406	10	Depth	140	140	140	184	184	235	235	286	286	337
		Deflection	L/681	L/352	L/203	L/300	L/201	L/298	L/217	L/296	L/228	L/295
	20	Depth	140	140	140	184	184	235	235	286	286	337
		Deflection	L/621	L/323	L/185	L/281	L/187	L/283	L/205	L/284	L/218	L/284
	30	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/568	L/297	L/417	L/263	L/382	L/268	L/194	L/272	L/208	L/274
	40	Depth	140	140	184	184	235	235	235	286	286	337
		Deflection	L/520	L/272	L/391	L/246	L/363	L/255	L/184	L/260	L/199	L/265
	50	Depth	140	140	184	184	235	235	286	286	286	337
		Deflection	L/479	L/249	L/367	L/230	L/345	L/242	L/333	L/249	L/190	L/255
610	10	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/448	L/230	L/313	L/197	L/279	L/196	L/260	L/195	L/248	L/195
	20	Depth	140	140	184	184	235	235	286	286	337	337
		Deflection	L/403	L/206	L/289	L/181	L/262	L/183	L/247	L/185	L/237	L/186
	30	Depth	140	140	184	235	235	286	286	337	337	N/A
		Deflection	L/363	L/185	L/267	L/367	L/246	L/322	L/234	L/295	L/227	N/A
	40	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/328	L/421	L/246	L/345	L/231	L/306	L/222	L/282	L/217	N/A
	50	Depth	140	184	184	235	235	286	286	337	337	N/A
		Deflection	L/296	L/389	L/227	L/324	L/217	L/290	L/211	L/270	L/207	N/A

Notes:

- The designer must assure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact LP at 1-888-820-0325.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with minimum 9.5mm thick plywood or OSB and fastened to meet the requirements of the National Building Code of Canada, unless greater requirements are specified by the project engineer. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada.
- Full depth blocking is required at 2.4 m on centre, unless greater requirements are specified by the project engineer.
- The wall plates are assumed to be of the same material as the studs. The resistance of the wall plates must be checked in accordance with CSA O86.
- The connection between the studs and the wall plates must be designed by the project engineer.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	337
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/4

Table 2.10 - Nordic Lam Wall Studs

Wind pressure $q_{1/50}$ 0.65 kPa



Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		Nordic Lam ES11 Grade									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	184	184	235	235	286	286	286	343
		Deflection	L/560	L/288	L/388	L/244	L/344	L/242	L/319	L/240	L/184	L/253
	20	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/520	L/268	L/368	L/231	L/330	L/232	L/309	L/232	L/312	L/245
	30	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/484	L/250	L/349	L/219	L/317	L/222	L/298	L/224	L/303	L/238
	40	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/451	L/233	L/331	L/207	L/304	L/212	L/288	L/216	L/295	L/231
	50	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/421	L/217	L/314	L/196	L/292	L/203	L/279	L/208	L/287	L/225
406	10	Depth	140	140	184	184	235	286	286	343	343	343
		Deflection	L/417	L/214	L/289	L/182	L/257	L/327	L/239	L/312	L/240	L/189
	20	Depth	140	140	184	235	235	286	286	343	343	343
		Deflection	L/384	L/197	L/272	L/365	L/245	L/315	L/229	L/302	L/232	L/182
	30	Depth	140	140	184	235	235	286	286	343	343	381
		Deflection	L/355	L/181	L/256	L/348	L/233	L/303	L/220	L/292	L/225	L/245
	40	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/328	L/413	L/241	L/332	L/222	L/291	L/211	L/283	L/217	L/238
	50	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/303	L/389	L/226	L/316	L/211	L/280	L/203	L/273	L/210	L/231
610	10	Depth	140	184	184	235	286	286	343	343	381	N/A
		Deflection	L/273	L/328	L/190	L/252	L/307	L/216	L/274	L/206	L/219	N/A
	20	Depth	140	184	235	235	286	286	343	343	381	N/A
		Deflection	L/248	L/304	L/377	L/238	L/293	L/206	L/263	L/198	L/211	N/A
	30	Depth	140	184	235	235	286	286	343	343	381	N/A
		Deflection	L/224	L/282	L/355	L/224	L/279	L/196	L/253	L/190	L/203	N/A
	40	Depth	140	184	235	235	286	286	343	343	381	N/A
		Deflection	L/203	L/262	L/335	L/211	L/266	L/186	L/243	L/182	L/196	N/A
	50	Depth	140	184	235	235	286	343	343	381	381	N/A
		Deflection	L/184	L/244	L/316	L/199	L/254	L/320	L/233	L/246	L/188	N/A

Notes:

- Sizes shown in the table are based on dry service conditions.
- The designer must ensure that the design assumptions used to develop the table are appropriate for the application. See page 3 for stud table design assumptions. For additional design information, contact Nordic Engineered Wood at 1-866-817-3418.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with plywood, waferboard, or OSB of minimum 9.5 mm (3/8 inch) thickness, and fastened to meet the requirements of the National Building Code of Canada and the shear wall requirements for the application. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m (8 ft). The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	343	381
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/2	15

Table 2.10 (continued) - Nordic Lam Wall Studs



Wind pressure $q_{1/50}$ 0.65 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		Nordic Lam ES12 Grade									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	286	286	343
		Deflection	L/676	L/349	L/201	L/296	L/198	L/292	L/213	L/290	L/223	L/305
	20	Depth	140	140	140	184	184	235	235	286	286	343
		Deflection	L/631	L/327	L/188	L/282	L/188	L/281	L/204	L/281	L/216	L/297
	30	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/590	L/307	L/425	L/268	L/385	L/271	L/196	L/272	L/209	L/289
	40	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/553	L/288	L/405	L/255	L/371	L/260	L/188	L/264	L/202	L/282
	50	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/518	L/270	L/386	L/243	L/357	L/250	L/181	L/255	L/195	L/275
406	10	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/505	L/259	L/350	L/220	L/311	L/218	L/288	L/216	L/290	L/228
	20	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/468	L/241	L/331	L/208	L/297	L/208	L/278	L/208	L/281	L/221
	30	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/434	L/223	L/313	L/196	L/285	L/199	L/268	L/201	L/273	L/214
	40	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/404	L/207	L/296	L/185	L/272	L/190	L/259	L/193	L/265	L/208
	50	Depth	140	140	184	235	235	235	286	286	343	343
		Deflection	L/376	L/192	L/280	L/388	L/261	L/181	L/249	L/186	L/257	L/201
610	10	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/332	L/397	L/230	L/305	L/204	L/261	L/190	L/249	L/192	L/208
	20	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/303	L/370	L/215	L/290	L/193	L/250	L/182	L/240	L/184	L/201
	30	Depth	140	184	184	235	235	286	343	343	381	381
		Deflection	L/277	L/346	L/200	L/275	L/183	L/239	L/308	L/231	L/247	L/194
	40	Depth	140	184	184	235	286	286	343	343	381	381
		Deflection	L/254	L/323	L/186	L/260	L/325	L/229	L/297	L/223	L/239	L/187
	50	Depth	140	184	235	235	286	286	343	343	381	381
		Deflection	L/232	L/302	L/388	L/247	L/311	L/219	L/286	L/215	L/231	L/181

Notes:

- Sizes shown in the table are based on dry service conditions.
- The designer must ensure that the design assumptions used to develop the table are appropriate for the application. See page 3 for stud table design assumptions. For additional design information, contact Nordic Engineered Wood at 1-866-817-3418.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with plywood, waferboard, or OSB of minimum 9.5 mm (3/8 inch) thickness, and fastened to meet the requirements of the National Building Code of Canada and the shear wall requirements for the application. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m (8 ft). The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	343	381
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/2	15

Table 2.11 - Nordic Lam Wall Studs



Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		Nordic Lam ES11 Grade									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	286	286	343
		Deflection	L/655	L/338	L/195	L/288	L/192	L/285	L/207	L/283	L/217	L/298
	20	Depth	140	140	184	184	184	235	235	286	286	343
		Deflection	L/604	L/314	L/430	L/271	L/180	L/272	L/197	L/272	L/209	L/289
	30	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/558	L/291	L/406	L/256	L/370	L/260	L/188	L/262	L/201	L/280
	40	Depth	140	140	184	184	235	235	286	286	286	343
		Deflection	L/517	L/269	L/384	L/241	L/354	L/248	L/337	L/252	L/193	L/271
	50	Depth	140	140	184	184	235	235	286	286	286	343
		Deflection	L/480	L/250	L/362	L/227	L/338	L/237	L/324	L/243	L/186	L/263
406	10	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/488	L/251	L/340	L/214	L/302	L/212	L/281	L/211	L/283	L/222
	20	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/446	L/230	L/318	L/199	L/287	L/201	L/269	L/202	L/273	L/214
	30	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/409	L/210	L/298	L/186	L/272	L/190	L/258	L/193	L/263	L/207
	40	Depth	140	140	184	235	235	286	286	286	343	343
		Deflection	L/375	L/191	L/279	L/385	L/258	L/339	L/247	L/184	L/254	L/199
	50	Depth	140	184	184	235	235	286	286	343	343	343
		Deflection	L/345	L/444	L/261	L/365	L/245	L/325	L/236	L/319	L/245	L/192
610	10	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/320	L/385	L/223	L/297	L/199	L/254	L/185	L/243	L/187	L/202
	20	Depth	140	184	184	235	235	286	343	343	381	381
		Deflection	L/288	L/354	L/205	L/278	L/186	L/241	L/309	L/232	L/248	L/194
	30	Depth	140	184	184	235	286	286	343	343	381	381
		Deflection	L/259	L/327	L/188	L/261	L/325	L/229	L/296	L/222	L/238	L/187
	40	Depth	140	184	235	235	286	286	343	343	381	N/A
		Deflection	L/233	L/302	L/386	L/245	L/309	L/217	L/283	L/212	L/229	N/A
	50	Depth	140	184	235	235	286	286	343	343	381	N/A
		Deflection	L/209	L/279	L/362	L/230	L/293	L/205	L/271	L/203	L/220	N/A

Notes:

- Sizes shown in the table are based on dry service conditions.
- The designer must ensure that the design assumptions used to develop the table are appropriate for the application. See page 3 for stud table design assumptions. For additional design information, contact Nordic Engineered Wood at 1-866-817-3418.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with plywood, waferboard, or OSB of minimum 9.5 mm (3/8 inch) thickness, and fastened to meet the requirements of the National Building Code of Canada and the shear wall requirements for the application. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m (8 ft). The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	343	381
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/2	15

Table 2.11 (continued) - Nordic Lam Wall Studs



Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		Nordic Lam ES12 Grade									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/792	L/410	L/237	L/348	L/233	L/344	L/251	L/188	L/263	L/206
	20	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/733	L/382	L/220	L/330	L/220	L/330	L/240	L/330	L/254	L/199
	30	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/680	L/357	L/205	L/313	L/208	L/317	L/230	L/319	L/245	L/192
	40	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/633	L/333	L/190	L/297	L/197	L/304	L/220	L/308	L/237	L/185
	50	Depth	140	140	184	184	184	235	235	286	286	343
		Deflection	L/590	L/311	L/446	L/282	L/186	L/292	L/211	L/298	L/229	L/321
406	10	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/591	L/305	L/412	L/259	L/366	L/257	L/187	L/255	L/196	L/269
	20	Depth	140	140	184	184	235	235	286	286	286	343
		Deflection	L/543	L/281	L/387	L/244	L/349	L/245	L/327	L/245	L/188	L/260
	30	Depth	140	140	184	184	235	235	286	286	286	343
		Deflection	L/501	L/260	L/365	L/229	L/332	L/233	L/314	L/236	L/180	L/252
	40	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/462	L/239	L/343	L/215	L/317	L/222	L/302	L/226	L/310	L/243
	50	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/428	L/221	L/323	L/202	L/303	L/211	L/291	L/217	L/300	L/235
610	10	Depth	140	140	184	235	235	286	286	343	343	381
		Deflection	L/388	L/199	L/270	L/359	L/241	L/307	L/224	L/293	L/226	L/245
	20	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/352	L/431	L/251	L/339	L/227	L/293	L/213	L/282	L/217	L/236
	30	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/320	L/400	L/233	L/320	L/214	L/279	L/203	L/271	L/208	L/227
	40	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/291	L/372	L/216	L/302	L/201	L/266	L/193	L/260	L/200	L/219
	50	Depth	140	184	184	235	235	286	286	343	381	381
		Deflection	L/264	L/346	L/200	L/285	L/189	L/254	L/184	L/250	L/270	L/211

Notes:

- Sizes shown in the table are based on dry service conditions.
- The designer must ensure that the design assumptions used to develop the table are appropriate for the application. See page 3 for stud table design assumptions. For additional design information, contact Nordic Engineered Wood at 1-866-817-3418.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with plywood, waferboard, or OSB of minimum 9.5 mm (3/8 inch) thickness, and fastened to meet the requirements of the National Building Code of Canada and the shear wall requirements for the application. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m (8 ft). The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	343	381
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/2	15

Table 2.12 - Nordic Lam Wall Studs

Wind pressure $q_{1/50}$ 0.45 kPa



Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		Nordic Lam ES11 Grade									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/790	L/410	L/237	L/349	L/234	L/346	L/252	L/189	L/265	L/208
	20	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/720	L/377	L/217	L/328	L/219	L/329	L/239	L/330	L/254	L/199
	30	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/659	L/347	L/198	L/308	L/204	L/313	L/227	L/317	L/244	L/190
	40	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/604	L/319	L/180	L/289	L/190	L/298	L/216	L/304	L/233	L/182
	50	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/556	L/294	L/428	L/271	L/403	L/283	L/204	L/292	L/223	L/316
406	10	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/589	L/304	L/412	L/260	L/367	L/258	L/187	L/257	L/197	L/271
	20	Depth	140	140	184	184	235	235	286	286	286	343
		Deflection	L/532	L/276	L/383	L/241	L/347	L/243	L/326	L/245	L/188	L/260
	30	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/483	L/250	L/356	L/223	L/327	L/229	L/311	L/233	L/319	L/250
	40	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/439	L/227	L/331	L/207	L/309	L/216	L/297	L/222	L/306	L/240
	50	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/400	L/205	L/308	L/191	L/292	L/203	L/283	L/211	L/294	L/231
610	10	Depth	140	140	184	235	235	286	286	343	343	381
		Deflection	L/386	L/197	L/270	L/360	L/241	L/309	L/225	L/295	L/227	L/246
	20	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/343	L/424	L/247	L/335	L/225	L/291	L/212	L/281	L/216	L/236
	30	Depth	140	184	184	235	235	286	286	343	381	381
		Deflection	L/305	L/387	L/225	L/313	L/209	L/275	L/200	L/268	L/287	L/226
	40	Depth	140	184	184	235	235	286	286	343	381	381
		Deflection	L/272	L/355	L/206	L/292	L/194	L/260	L/188	L/255	L/275	L/216
	50	Depth	140	184	184	235	235	286	343	381	381	381
		Deflection	L/243	L/325	L/187	L/272	L/180	L/245	L/323	L/341	L/263	L/206

Notes:

- Sizes shown in the table are based on dry service conditions.
- The designer must ensure that the design assumptions used to develop the table are appropriate for the application. See page 3 for stud table design assumptions. For additional design information, contact Nordic Engineered Wood at 1-866-817-3418.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with plywood, waferboard, or OSB of minimum 9.5 mm (3/8 inch) thickness, and fastened to meet the requirements of the National Building Code of Canada and the shear wall requirements for the application. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m (8 ft). The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	343	381
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/2	15

Table 2.12 (continued) - Nordic Lam Wall Studs



Wind pressure $q_{1/50}$ 0.45 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		Nordic Lam ES12 Grade									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	140	140	140	184	184	184	235	235	286	286
		Deflection	L/955	L/497	L/288	L/423	L/283	L/198	L/305	L/229	L/320	L/252
	20	Depth	140	140	140	184	184	184	235	235	286	286
		Deflection	L/874	L/460	L/266	L/399	L/267	L/186	L/291	L/218	L/308	L/242
	30	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/803	L/426	L/246	L/377	L/251	L/382	L/278	L/208	L/297	L/233
	40	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/740	L/395	L/227	L/356	L/237	L/365	L/266	L/198	L/286	L/224
	50	Depth	140	140	140	184	184	235	235	235	286	286
		Deflection	L/684	L/367	L/209	L/336	L/222	L/349	L/253	L/188	L/275	L/215
406	10	Depth	140	140	140	184	184	235	235	286	286	286
		Deflection	L/713	L/369	L/213	L/315	L/210	L/312	L/227	L/311	L/239	L/188
	20	Depth	140	140	140	184	184	235	235	286	286	343
		Deflection	L/648	L/338	L/194	L/295	L/196	L/296	L/215	L/297	L/229	L/316
	30	Depth	140	140	184	184	184	235	235	286	286	343
		Deflection	L/591	L/310	L/436	L/275	L/182	L/281	L/203	L/285	L/218	L/305
	40	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/541	L/284	L/408	L/257	L/379	L/266	L/192	L/273	L/209	L/294
	50	Depth	140	140	184	184	235	235	235	286	286	343
		Deflection	L/496	L/260	L/382	L/240	L/360	L/253	L/181	L/261	L/199	L/283
610	10	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/468	L/241	L/328	L/206	L/292	L/205	L/272	L/204	L/275	L/216
	20	Depth	140	140	184	184	235	235	286	286	343	343
		Deflection	L/420	L/215	L/302	L/189	L/274	L/192	L/258	L/193	L/263	L/206
	30	Depth	140	140	184	235	235	286	286	286	343	343
		Deflection	L/377	L/192	L/278	L/383	L/257	L/336	L/245	L/183	L/252	L/197
	40	Depth	140	184	184	235	235	286	286	343	343	343
		Deflection	L/340	L/437	L/257	L/359	L/241	L/319	L/232	L/313	L/241	L/188
	50	Depth	140	184	184	235	235	286	286	343	343	381
		Deflection	L/307	L/404	L/236	L/337	L/226	L/303	L/220	L/299	L/230	L/254

Notes:

- Sizes shown in the table are based on dry service conditions.
- The designer must ensure that the design assumptions used to develop the table are appropriate for the application. See page 3 for stud table design assumptions. For additional design information, contact Nordic Engineered Wood at 1-866-817-3418.
- Both faces of the stud must be laterally supported by sheathing. At least one face of the stud must be sheathed with plywood, waferboard, or OSB of minimum 9.5 mm (3/8 inch) thickness, and fastened to meet the requirements of the National Building Code of Canada and the shear wall requirements for the application. The other face must be sheathed with either structural sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking is 2.4 m (8 ft). The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	140	184	235	286	343	381
depth inches	5-1/2	7-1/4	9-1/4	11-1/4	13-1/2	15

**Table 2.13 -
TEMLAM 2850f-1.9E Studs by Jager EWP**



Wind pressure $q_{1/50}$ 0.65 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		2850f-1.9E Temlam									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/1098	L/572	L/333	L/209	L/296	L/208	L/276	L/207	L/188	L/244
	20	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/1018	L/538	L/314	L/197	L/283	L/198	L/266	L/199	L/181	L/236
	30	Depth	184	184	184	184	235	235	286	286	318	356
		Deflection	L/947	L/507	L/297	L/186	L/271	L/189	L/256	L/192	L/205	L/229
	40	Depth	184	184	184	235	235	235	286	286	318	356
		Deflection	L/884	L/478	L/281	L/386	L/259	L/180	L/247	L/184	L/198	L/223
	50	Depth	184	184	184	235	235	241	286	292	318	356
		Deflection	L/828	L/452	L/265	L/369	L/248	L/187	L/238	L/190	L/192	L/216
406	10	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/822	L/427	L/248	L/330	L/221	L/282	L/206	L/182	L/232	L/182
	20	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/759	L/399	L/232	L/313	L/210	L/271	L/197	L/205	L/224	L/263
	30	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/703	L/374	L/217	L/298	L/199	L/259	L/188	L/197	L/216	L/256
	40	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/654	L/350	L/203	L/283	L/188	L/249	L/180	L/190	L/209	L/248
	50	Depth	184	184	184	235	241	286	292	318	356	406
		Deflection	L/609	L/328	L/189	L/269	L/194	L/238	L/185	L/182	L/202	L/241
610	10	Depth	184	184	235	235	286	286	318	356	406	
		Deflection	L/543	L/281	L/344	L/217	L/265	L/186	L/187	L/199	L/228	
	20	Depth	184	184	235	235	286	292	356	356	406	
		Deflection	L/497	L/259	L/323	L/204	L/252	L/188	L/254	L/190	L/220	
	30	Depth	184	184	235	235	286	302	356	356	406	
		Deflection	L/457	L/239	L/303	L/191	L/239	L/199	L/243	L/182	L/212	
	40	Depth	184	184	235	241	286	302	356	406	406	
		Deflection	L/421	L/221	L/285	L/194	L/227	L/189	L/233	L/265	L/204	
	50	Depth	184	184	235	241	286	318	356	406	406	
		Deflection	L/389	L/204	L/268	L/183	L/215	L/213	L/224	L/256	L/197	

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Jager EWP at 1-800-387-7060
- It is recommended that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended. The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	184	235	241	286	292	302	318	356	406
depth inches	7-1/4	9-1/4	9-1/2	11-1/4	11-1/2	11-7/8	12-1/2	14	16

Table 2.13 (continued) -
TEMLAM 3300f-2.0E Studs by Jager EWP



Wind pressure $q_{1/50}$ 0.65 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		3300f-2.0E Temlam									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	184	184	184	184	235	235	286	286	302	318
		Deflection	L/1158	L/603	L/351	L/221	L/312	L/219	L/291	L/218	L/198	L/182
	20	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/1074	L/568	L/332	L/209	L/299	L/210	L/280	L/210	L/191	L/250
	30	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/1000	L/536	L/314	L/197	L/286	L/200	L/270	L/203	L/184	L/242
	40	Depth	184	184	184	184	235	235	286	286	356	356
		Deflection	L/934	L/506	L/297	L/185	L/274	L/191	L/261	L/195	L/300	L/235
	50	Depth	184	184	184	235	235	235	286	286	356	356
		Deflection	L/875	L/478	L/281	L/390	L/262	L/182	L/252	L/188	L/291	L/229
406	10	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/866	L/451	L/262	L/348	L/233	L/298	L/217	L/192	L/244	L/192
	20	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/801	L/422	L/245	L/331	L/221	L/286	L/208	L/185	L/236	L/185
	30	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/743	L/395	L/230	L/315	L/210	L/274	L/199	L/209	L/228	L/270
	40	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/691	L/371	L/215	L/299	L/200	L/263	L/191	L/201	L/221	L/262
	50	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/645	L/348	L/202	L/285	L/189	L/252	L/183	L/193	L/213	L/255
610	10	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/572	L/296	L/363	L/229	L/280	L/196	L/198	L/209	L/241	L/189
	20	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/525	L/274	L/341	L/215	L/266	L/186	L/189	L/201	L/232	L/182
	30	Depth	184	184	235	235	286	292	318	356	406	
		Deflection	L/483	L/253	L/321	L/202	L/253	L/189	L/180	L/193	L/224	
	40	Depth	184	184	235	235	286	302	356	356	406	
		Deflection	L/446	L/234	L/302	L/190	L/240	L/200	L/247	L/185	L/216	
	50	Depth	184	184	235	241	286	302	356	406	406	
		Deflection	L/412	L/217	L/284	L/194	L/228	L/191	L/237	L/271	L/208	

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Jager EWP at 1-800-387-7060
- It is recommended that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended. The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	184	235	241	286	292	302	318	356	406
depth inches	7-1/4	9-1/4	9-1/2	11-1/4	11-1/2	11-7/8	12-1/2	14	16

**Table 2.14 -
TEMLAM 2850f-1.9E Studs by Jager EWP**



Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		2850f-1.9E Temlam									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	184	184	184	184	235	235	286	286	286	318
		Deflection	L/1282	L/671	L/391	L/246	L/349	L/245	L/325	L/244	L/187	L/204
	20	Depth	184	184	184	184	235	235	286	286	292	318
		Deflection	L/1177	L/627	L/368	L/231	L/332	L/233	L/312	L/234	L/192	L/196
	30	Depth	184	184	184	184	235	235	286	286	292	318
		Deflection	L/1085	L/587	L/346	L/217	L/316	L/222	L/300	L/225	L/184	L/189
	40	Depth	184	184	184	184	235	235	286	286	302	318
		Deflection	L/1005	L/550	L/325	L/203	L/302	L/211	L/288	L/215	L/197	L/182
	50	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/934	L/517	L/306	L/190	L/287	L/200	L/277	L/207	L/189	L/252
406	10	Depth	184	184	184	184	235	235	286	286	318	356
		Deflection	L/960	L/501	L/291	L/183	L/260	L/182	L/242	L/182	L/193	L/215
	20	Depth	184	184	184	235	235	241	286	302	318	356
		Deflection	L/877	L/465	L/271	L/366	L/246	L/186	L/231	L/205	L/185	L/207
	30	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/805	L/432	L/252	L/347	L/232	L/303	L/221	L/196	L/253	L/199
	40	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/743	L/403	L/235	L/328	L/219	L/290	L/210	L/187	L/244	L/191
	50	Depth	184	184	184	235	235	286	286	318	356	356
		Deflection	L/687	L/375	L/218	L/310	L/207	L/277	L/201	L/212	L/235	L/184
610	10	Depth	184	184	184	235	241	286	302	356	406	406
		Deflection	L/634	L/329	L/190	L/255	L/184	L/219	L/188	L/234	L/269	L/211
	20	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/574	L/302	L/377	L/238	L/295	L/207	L/210	L/223	L/258	L/203
	30	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/523	L/277	L/351	L/222	L/279	L/195	L/199	L/213	L/248	L/195
	40	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/478	L/254	L/328	L/207	L/263	L/184	L/189	L/204	L/239	L/187
	50	Depth	184	184	235	235	286	292	356	356	406	
		Deflection	L/438	L/233	L/307	L/193	L/249	L/186	L/260	L/195	L/229	

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Jager EWP at 1-800-387-7060
- It is recommended that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended. The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	184	235	241	286	292	302	318	356	406
depth inches	7-1/4	9-1/4	9-1/2	11-1/4	11-1/2	11-7/8	12-1/2	14	16

Table 2.14 (continued) -
TEMLAM 3300f-2.0E Studs by Jager EWP



Wind pressure $q_{1/50}$ 0.55 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		3300f-2.0E Temlam									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	184	184	184	184	235	235	235	286	286	302
		Deflection	L/1352	L/707	L/413	L/260	L/368	L/258	L/188	L/257	L/198	L/183
	20	Depth	184	184	184	184	235	235	241	286	286	318
		Deflection	L/1241	L/662	L/388	L/244	L/351	L/246	L/193	L/247	L/190	L/207
	30	Depth	184	184	184	184	235	235	241	286	286	318
		Deflection	L/1145	L/620	L/366	L/230	L/335	L/234	L/184	L/238	L/182	L/200
	40	Depth	184	184	184	184	235	235	286	286	292	318
		Deflection	L/1061	L/582	L/344	L/216	L/319	L/223	L/305	L/228	L/187	L/192
	50	Depth	184	184	184	184	235	235	286	286	302	318
		Deflection	L/987	L/547	L/324	L/202	L/305	L/212	L/293	L/219	L/200	L/185
406	10	Depth	184	184	184	184	235	235	286	286	318	356
		Deflection	L/1012	L/528	L/307	L/193	L/274	L/192	L/256	L/192	L/204	L/226
	20	Depth	184	184	184	235	235	235	286	286	318	356
		Deflection	L/925	L/491	L/287	L/387	L/260	L/181	L/244	L/183	L/196	L/218
	30	Depth	184	184	184	235	235	241	286	292	318	356
		Deflection	L/850	L/457	L/267	L/366	L/246	L/186	L/233	L/186	L/187	L/210
	40	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/785	L/426	L/249	L/347	L/232	L/307	L/223	L/199	L/258	L/202
	50	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/727	L/398	L/232	L/329	L/220	L/293	L/213	L/190	L/249	L/195
610	10	Depth	184	184	184	235	241	286	302	356	356	406
		Deflection	L/668	L/348	L/201	L/269	L/195	L/231	L/199	L/247	L/190	L/223
	20	Depth	184	184	184	235	241	286	302	356	356	406
		Deflection	L/607	L/319	L/184	L/252	L/182	L/219	L/188	L/236	L/181	L/214
	30	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/553	L/293	L/372	L/235	L/295	L/207	L/211	L/226	L/262	L/206
	40	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/506	L/270	L/348	L/220	L/279	L/195	L/200	L/216	L/252	L/198
	50	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/465	L/248	L/326	L/206	L/264	L/184	L/190	L/206	L/243	L/190

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Jager EWP at 1-800-387-7060
- It is recommended that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended. The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	184	235	241	286	292	302	318	356	406
depth inches	7-1/4	9-1/4	9-1/2	11-1/4	11-1/2	11-7/8	12-1/2	14	16

**Table 2.15 -
TEMLAM 2850f-1.9E Studs by Jager EWP**



Wind pressure $q_{1/50}$ 0.45 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		2850f-1.9E Temlam									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	184	184	184	184	184	235	235	286	286	292
		Deflection	L/1541	L/811	L/474	L/299	L/200	L/298	L/217	L/297	L/228	L/191
	20	Depth	184	184	184	184	184	235	235	286	286	292
		Deflection	L/1394	L/750	L/443	L/279	L/186	L/282	L/205	L/284	L/218	L/182
	30	Depth	184	184	184	184	235	235	235	286	286	302
		Deflection	L/1269	L/696	L/413	L/261	L/381	L/267	L/193	L/272	L/208	L/194
	40	Depth	184	184	184	184	235	235	235	286	286	302
		Deflection	L/1163	L/647	L/386	L/243	L/361	L/253	L/182	L/260	L/199	L/185
	50	Depth	184	184	184	184	235	235	241	286	286	318
		Deflection	L/1071	L/603	L/361	L/226	L/342	L/239	L/187	L/248	L/189	L/210
406	10	Depth	184	184	184	184	235	235	286	286	292	318
		Deflection	L/1153	L/605	L/353	L/222	L/316	L/222	L/295	L/221	L/181	L/185
	20	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/1039	L/556	L/326	L/205	L/297	L/208	L/280	L/210	L/191	L/251
	30	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/942	L/513	L/302	L/188	L/279	L/195	L/266	L/199	L/181	L/241
	40	Depth	184	184	184	235	235	235	286	286	318	356
		Deflection	L/860	L/474	L/279	L/390	L/262	L/182	L/253	L/188	L/204	L/231
	50	Depth	184	184	184	235	235	241	286	292	318	356
		Deflection	L/788	L/438	L/258	L/367	L/246	L/186	L/240	L/192	L/195	L/221
610	10	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/761	L/398	L/231	L/309	L/207	L/266	L/194	L/201	L/219	L/257
	20	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/680	L/361	L/209	L/287	L/191	L/250	L/181	L/190	L/208	L/246
	30	Depth	184	184	184	235	241	286	292	356	356	406
		Deflection	L/612	L/328	L/189	L/266	L/192	L/235	L/182	L/257	L/198	L/236
	40	Depth	184	184	235	235	286	286	302	356	356	406
		Deflection	L/553	L/298	L/388	L/247	L/314	L/220	L/191	L/245	L/188	L/225
	50	Depth	184	184	235	235	286	286	318	356	406	406
		Deflection	L/503	L/272	L/360	L/229	L/295	L/207	L/214	L/233	L/274	L/215

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Jager EWP at 1-800-387-7060
- It is recommended that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended. The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	184	235	241	286	292	302	318	356	406
depth inches	7-1/4	9-1/4	9-1/2	11-1/4	11-1/2	11-7/8	12-1/2	14	16

Table 2.15 (continued) -
TEMLAM 3300f-2.0E Studs by Jager EWP



Wind pressure $q_{1/50}$ 0.45 kPa

Depth required (mm) for 44 mm (1-3/4") thick studs

Stud spacing mm	Factored axial load kN/m		3300f-2.0E Temlam									
			Stud length									
			3.66m (12 ft)	4.57m (15 ft)	5.49m (18 ft)	6.40m (21 ft)	7.32m (24 ft)	8.23m (27 ft)	9.14m (30 ft)	10.06m (33 ft)	10.97m (36 ft)	11.89m (39 ft)
305	10	Depth	184	184	184	184	184	235	235	241	286	286
		Deflection	L/1624	L/855	L/500	L/316	L/211	L/314	L/229	L/185	L/241	L/189
	20	Depth	184	184	184	184	184	235	235	286	286	286
		Deflection	L/1470	L/791	L/467	L/295	L/196	L/298	L/216	L/300	L/230	L/180
	30	Depth	184	184	184	184	184	235	235	286	286	292
		Deflection	L/1340	L/735	L/437	L/276	L/183	L/283	L/205	L/287	L/220	L/184
	40	Depth	184	184	184	184	235	235	235	286	286	302
		Deflection	L/1228	L/684	L/409	L/258	L/382	L/268	L/194	L/275	L/211	L/196
	50	Depth	184	184	184	184	235	235	235	286	286	302
		Deflection	L/1132	L/639	L/383	L/241	L/363	L/254	L/183	L/263	L/201	L/188
406	10	Depth	184	184	184	184	235	235	241	286	292	318
		Deflection	L/1216	L/639	L/373	L/235	L/333	L/234	L/184	L/233	L/191	L/195
	20	Depth	184	184	184	184	235	235	286	286	292	318
		Deflection	L/1096	L/588	L/345	L/217	L/314	L/220	L/296	L/222	L/182	L/186
	30	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/995	L/542	L/320	L/200	L/295	L/206	L/282	L/211	L/192	L/254
	40	Depth	184	184	184	184	235	235	286	286	302	356
		Deflection	L/909	L/502	L/296	L/184	L/278	L/194	L/268	L/200	L/183	L/244
	50	Depth	184	184	184	235	235	235	286	286	318	356
		Deflection	L/834	L/465	L/275	L/389	L/262	L/181	L/255	L/190	L/207	L/234
610	10	Depth	184	184	184	235	235	286	286	302	356	356
		Deflection	L/803	L/420	L/244	L/327	L/219	L/281	L/204	L/181	L/231	L/181
	20	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/718	L/382	L/222	L/303	L/203	L/264	L/192	L/201	L/220	L/260
	30	Depth	184	184	184	235	235	286	286	318	356	406
		Deflection	L/647	L/348	L/201	L/282	L/188	L/249	L/180	L/190	L/209	L/249
	40	Depth	184	184	184	235	241	286	292	356	356	406
		Deflection	L/586	L/317	L/182	L/262	L/189	L/234	L/181	L/259	L/199	L/239
	50	Depth	184	184	235	235	286	286	302	356	356	406
		Deflection	L/533	L/289	L/382	L/243	L/313	L/220	L/191	L/247	L/189	L/228

Notes:

- The designer must ensure that the assumptions used to develop the tables are appropriate for the application. See Page 3 for stud table assumptions. For additional design information, contact Jager EWP at 1-800-387-7060
- It is recommended that both faces of the studs be covered by sheathing or cladding. At least one face of the stud should be sheathed with 9.5 mm or thicker plywood or OSB and fastened to meet the requirements of the National Building Code of Canada. The other face may be sheathed with cladding, sheathing or drywall meeting the requirements of the National Building Code of Canada. The sheathing and fastening must meet the shearwall requirements for the application.
- Maximum spacing of full depth blocking of 2.4 m is recommended. The blocking must meet the shearwall requirements for the application.
- Imperial equivalents for the stud depths are:

depth mm	184	235	241	286	292	302	318	356	406
depth inches	7-1/4	9-1/4	9-1/2	11-1/4	11-1/2	11-7/8	12-1/2	14	16

3. Example

There are many aspects of wall construction that must be considered in a Tall Wall design. As a minimum, the following must be accounted for:

- Design of the studs
- Design of the stud connections
- Shearwall design including; overturning/hold-down design, shear panel design, shearwall chord design, base plate anchorage and drag strut design
- Design of the members around wall openings including; lintel design; jack post stud design, king post stud design and the design of the connections.
- Non-structural aspects of wall design including fire and thermal resistance.

This design example is based on the Crestbrook Value Added Centre built in 1999/2000. The example uses design assumptions outlined in the *National Building Code of Canada, CSA O86.1 (2005) Engineering Design in Wood (Limit States Design)* and Tembec's proprietary design information for TEMPLAM™ 2.0E stud.

Details in the design example are not necessarily the same as the final details used in the building construction. The details shown here have been adapted for more general building assumptions.

3.1 Overview of Building

Crestbrook Forest Industries is a lumber manufacturing facility in Cranbrook British Columbia. Additional space was required for their lumber remanufacturing and finger-joining operations. The facilities required large open areas without columns. As well, the North wall could not be load-bearing so that future plant expansion could be accommodated. Originally, a steel structure was specified but Tembec Forest Products, Crestbrook's parent company had recently adopted a policy which required wood to be considered for all their construction and used where cost effective. Analysis indicated a wood building could be constructed for the same cost as the pre-engineered steel building originally specified.

The building is a 2100 m² (22,300 ft²) one storey wood frame with a concrete slab on grade floor and foundation. Figure 3.1 gives an overview of the building.

Figure 3.1
Isometric diagram of
new building

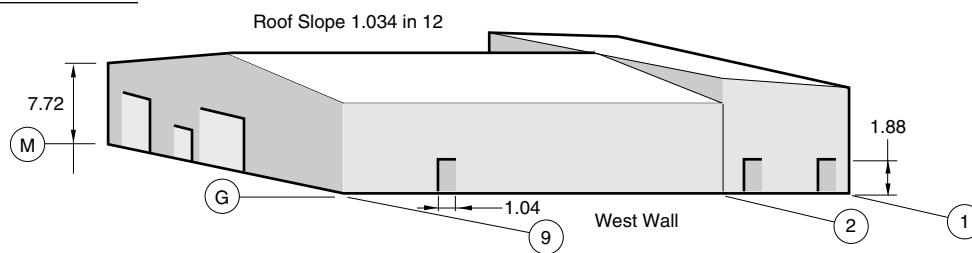
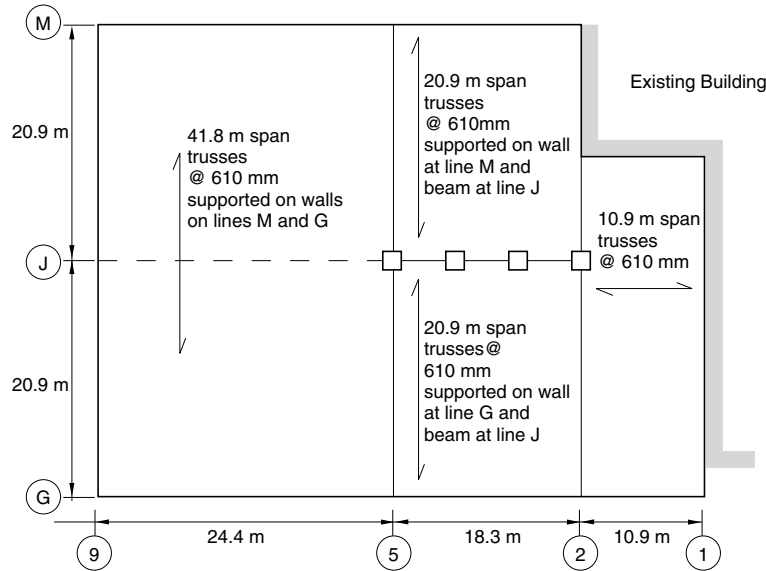


Figure 3.2
Roof framing plan



A roof framing plan is illustrated in Figure 3.2. The west wall, “Wall G” will be used for this example. The wall is 7.72 m (25 ft 4 in) tall and at the north end supports trusses spanning 41.8 m (137 ft).

Cranbrook has the following design data:

- Specified ground snow load, S_g , 3.0 kPa
- Associated rain load, S_r , 0.2 kPa
- 1/50 hourly wind pressure, $q_{1/50}$, 0.33 kPa
- Seismic design loads are minimal and did not affect the design of this structure.

3.2 Stud Design

Studs used in this project were 44 x 286 mm (1-3/4 x 11-1/4 in) TemLam™ 2.0E studs manufactured by Tembec. Studs were spaced at 610 mm o/c and blocked at 1220 mm. Figure 3.3 shows a typical wall section. The stud length is the height of the wall minus the thickness of the top and bottom plates – 7.59 m. This stud design example will be for studs supporting the 41.8 m span trusses.

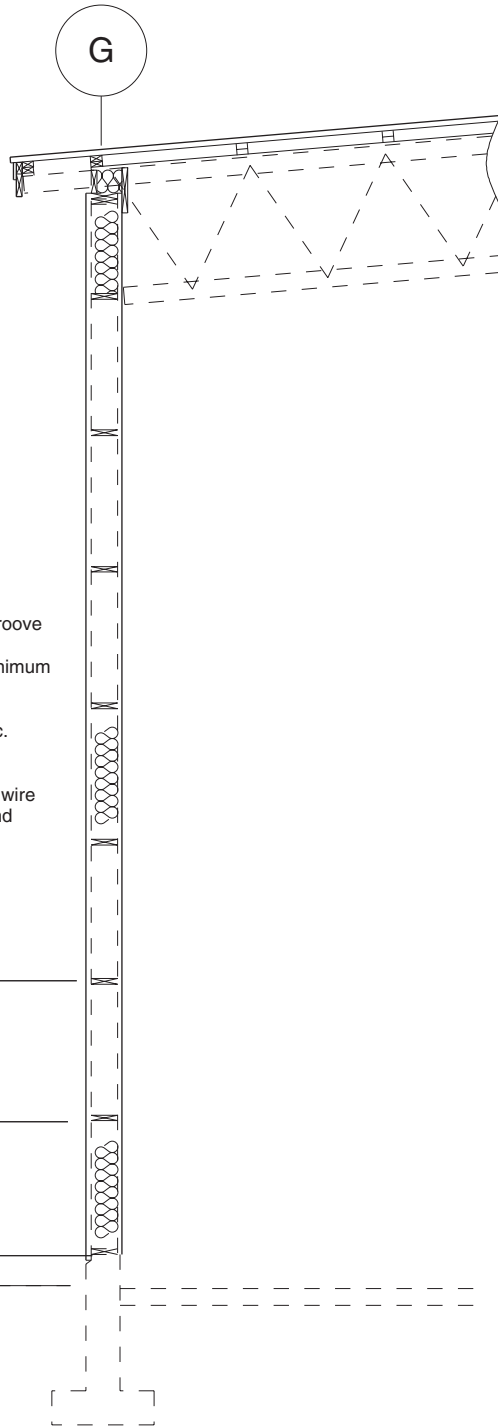
Load information

Stud axial loads

Roof dead load

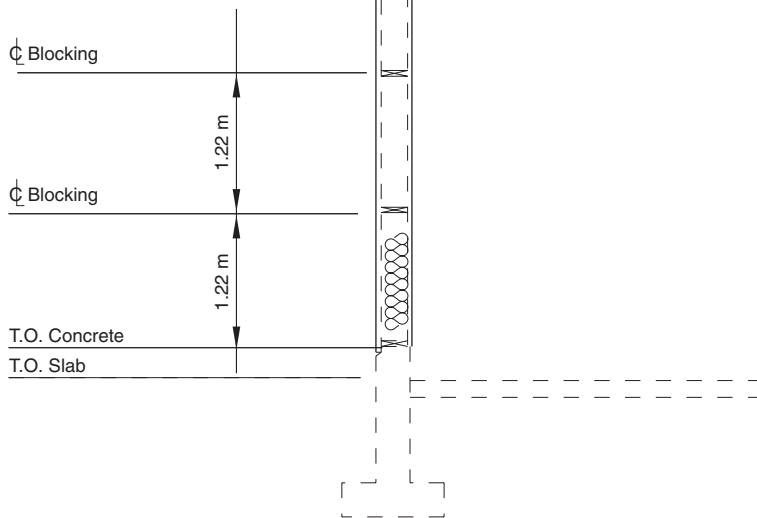
Specified roof dead load	= 0.718 kPa
Roof load tributary width	= truss span/2 = 20.9 m
Specified roof dead load on wall	= 0.718 x 20.9 = 15.0 kN/m
Factored roof dead load on wall	= 1.4 x 15.0 = 21.0 kN/m (dead alone)
	= 1.25 x 15.0 = 18.8 kN/m (combined)

Figure 3.3
Typical wall section



Typical Wall Construction

- 38 X 140 mm horizontal tongue and groove siding. Fasten with 3 1/4" galvanized common wire nails @ 150 mm o.c. minimum
- Approved building paper
- 44 x 286 mm 2.0E LVL studs
- 38 x 286 mm blocking @ 1220 mm o.c.
- R20 fiberglass batt insulation
- 6 mil poly vapour barrier
- 9.5 mm OSB. Fasten with 2" common wire nails @ 150 mm o.c. at panel edges and 300 mm o.c. along intermediate framing members



Wall dead load

Specified wall dead load = 0.40 kPa

The critical section for combined bending and axial loads on a stud is generally the mid-height of the stud. Therefore, consider half of the wall dead weight in the stud design.


Tributary height of wall dead load = $7.72/2 = 3.86$ m

Specified wall dead load = 0.40×3.86
= 1.54 kN/m

Factored wall dead load = 1.4×1.54
= 2.16 kN/m (dead alone)


= 1.25×1.54
= 1.93 kN/m (combined)


Roof snow load, S

$S = I_s \times [S_s(C_b C_w C_s C_a) + S_r]$  4.1.6

Importance factor (ULS) $I_s = 1.0$

Importance factor(SLS) $I_s = 0.9$

Ground snow load $S_s = 3.0$ kPa  Appendix C

Associated rain load $S_r = 0.2$ kPa  Appendix C

Basic roof snow factor $C_b = 0.8$

All other factors $C_w, C_s, C_a = 1.0$

$S = 3.0 \times (0.8 \times 1 \times 1 \times 1) + 0.2$
= 2.6 kPa

Specified snow load on wall = 2.6×20.9
= 54.3 kN/m

Factored snow load on wall (principal) = 1.5×54.4
= 81.5 kN/m

Factored snow load on wall (companion) = 0.5×54.4
= 27.2 kN/m

Table 3.1
Summary of axial loads

	Specified Load	Factored Load
Wall + Roof Dead Load	16.6 kN/m	23.2 kN/m (dead alone) 20.7 kN/m (combined)
Snow Load (principal)	54.3 kN/m	81.5 kN/m
Snow Load (companion)	54.3 kN/m	27.2 kN/m
Stud Dead Load	10.1 kN	14.1 kN (dead alone) 12.6 kN/m (combined)
Stud Snow Load (Principal)	33.1 kN	49.7 kN
Stud Snow Load (Companion)	33.1 kN	16.6 kN
Total Stud Load (snow Principal)	43.2 kN	62.3 kN
Total Stud Load (snow Companion)	43.2 kN	29.2 kN
Stud Load, deflection (Principal)	39.9 kN	NA
Stud Load deflection (Companion)	25.0 kN	NA

NA: Not applicable

Stud wind loads

$$p = qC_e C_g C_p \pm qC_e C_{gi} C_{pi} \quad \text{NBCC 4.1.7}$$

Wind load for strength	$q_{1/50} = 0.33 \text{ kPa}$	NBCC Appendix C
Importance factor (ULS)	$I_w = 1.0$	
Importance factor (SLS)	$I_w = 0.75$	
Exposure factor	$C_e = 0.7$	
External pressure coefficient and gust factor	$C_p C_g = -2.0$	NBCC Commentary I
Internal pressure coefficient	$C_{pi} = \pm 0.3$	
Internal gust factor	$C_{gi} = 2.0$	

Table 3.2
Summary of
wind loads

	Specified Load	Factored Load
Strength area load (principal)	0.601 kPa	0.841 kPa
Strength area load (companion)	0.601 kPa	0.240 kPa
Strength stud load (principal)	0.366 kN/m	0.513 kN/m
Strength stud load (companion)	0.366 kN/m	0.147 kN/m
Deflection stud load (principal)	0.275 kN/m	NA
Deflection stud load (companion)	0.110 kN/m	NA

NA: Not applicable

Stud resistance

Product design information for TEMLAM™ 2.0E – Available from Tembec

Specified bending strength	$f_b = 42.7 \text{ MPa}$
Specified shear strength	$f_v = 3.65 \text{ MPa}$
Specified compression parallel to grain strength	$f_c = 29.6 \text{ MPa}$
Specified compression perpendicular to grain strength	$f_{cp} = 7.24 \text{ MPa}$
Specified tension strength	$f_t = 29.0 \text{ MPa}$
Size factor for tension	$K_{zt} = 1$
Mean Modulus of Elasticity	$E_{50} = 13110 \text{ MPa}^*$
5th percentile Modulus of Elasticity ($0.87E_{50}$)	$E_{05} = 11400 \text{ MPa}^*$
Size factor in bending	$K_{zb} = (305/d)^{0.15} = 1.01$

* Published Modules of Elasticity values have been decreased 5% to account for shear deflection.

Modification factors

Bending resistance factor	$\phi = 0.9$	CSA 086.1	Supplement, 13.4
Shear resistance factor	$\phi = 0.9$		
Compression parallel to grain resistance factor	$\phi = 0.8$		
Compression perpendicular to grain resistance factor	$\phi = 0.8$		
Tension resistance factor	$\phi = 0.9$		
Load duration factor:			
Load combinations with wind	$K_D = 1.15$		
All other load combinations	$K_D = 1.00$		
System factor for bending	$K_H = 1.04$		
Length of bearing factor	$K_B = 1.19$	CSA 086.1	5.5
Size factor for bearing	$K_{Zcp} = 1.15$	CSA 086.1	5.5

Resistance of 44 x 286 mm stud of length 7.62 m CSA 086.1 Supplement, 13.4

With wind loads:

$$\begin{aligned}M_r &= \phi F_b S K_{zb} K_L \\ &= 27.8 \text{ kN}\cdot\text{m}\end{aligned}$$

$$\begin{aligned}V_r &= \phi F_v \frac{2}{3} A \\ &= 31.7 \text{ kN}\end{aligned}$$

$$\begin{aligned}P_r &= \phi F_c A K_{Zc} K_c \\ &= 132 \text{ kN}\end{aligned}$$

$$\begin{aligned}T_r &= \phi F_t A_n K_{Zt} \\ &= 359 \text{ kN (for a member with a 1/2 in dia. bolt)}\end{aligned}$$

Without wind loads:

$$\begin{aligned}M_r &= \phi F_b S K_{zb} K_L \\ &= 24.2 \text{ kN}\cdot\text{m}\end{aligned}$$

$$\begin{aligned}P_r &= \phi F_c A K_{Zc} K_c \\ &= 125 \text{ kN}\end{aligned}$$

$$\begin{aligned}Q'_r &= \left(\frac{2}{3}\right) \phi F_{cp} A'_b K_B K_{Zcp} \\ &= 75.5 \text{ kN}\end{aligned}$$

Note: At the top plate, a 16000 mm² steel bearing plate is provided at the truss support.

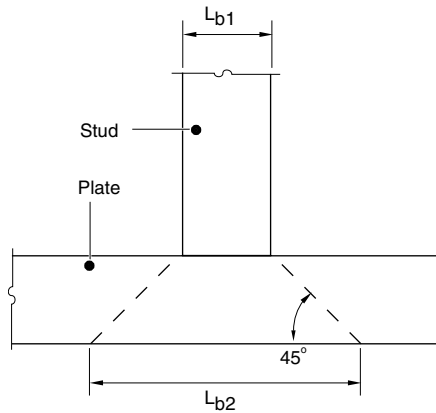
$$\begin{aligned}A'_b &= \frac{(16000 + 44 \times 286)}{2} \text{ but } \leq 1.5 \times 44 \times 286 \\ &= 14300 \text{ mm}^2\end{aligned}$$

At the bottom plate, axial load from the stud is assumed to be distributed through the sill plate at a 45° angle as shown in Figure 3.4.

$$A'_b = b \left[\frac{L_{b1} + L_{b2}}{2} \right], \text{ but } \leq 1.5 L_{b1}$$

$$= 18900 \text{ mm}^2 > 14300 \text{ Therefore, bearing of the top plate will govern}$$

Figure 3.4
Bearing of stud
on sill plate



Load Case 1 – axial loads alone (1.25 D +1.5 S)

$$P_f = 62.3 \text{ kN per stud}$$

Combined Loading:

Axial load may not be applied concentrically and is conservatively assumed to be applied at 1/6th the depth of the stud from the centre of the stud creating a moment as shown in Figure 3.5

The design should consider the more critical of:

- the unamplified moment at the top of the stud, and
- the amplified moment at the middle of the stud

(In the stud tables, the conservative case of amplified moment at the top of the stud was considered)

In this design example, the critical case is the amplified moment at the middle of the stud.

$$M'_f = \frac{1}{2} P_f \times \frac{d}{6}$$

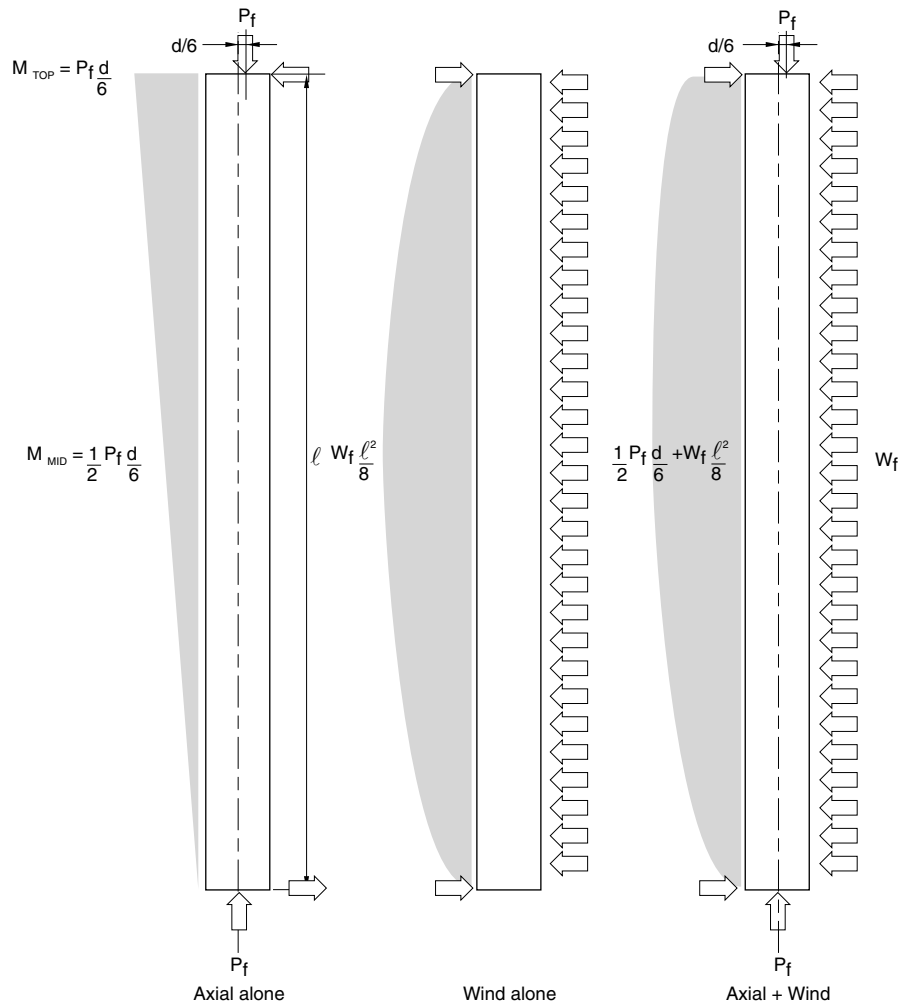
$$= 1.49 \text{ kN}\cdot\text{m per stud}$$

The following formula is used for the amplified moment due to eccentric load

$$\frac{P_f}{P_r} + \frac{M_f}{M_r} \leq 1.0$$

$$M_f = M'_f \left[\frac{1}{1 - \frac{P_f}{P_E}} \right]$$

Figure 3.5
**Eccentric load,
 lateral load and
 moments on
 the stud**



$$P_E = \frac{\pi^2 E_s I}{(K_e \ell)^2}$$

= 193 kN per stud

$$E_s I = 1120 \times 10^9 \text{ N}\cdot\text{mm}^2$$

$$M_f = 2.19 \text{ kN}\cdot\text{m per stud}$$

$$\frac{P_f}{P_r} + \frac{M_f}{M_r} \leq 1.0$$

= 0.6 ≤ 1.0 (Acceptable)

Bearing on top and bottom plates

$$Q_f = 62.3 \text{ kN} < 75.5 \text{ kN (Acceptable)}$$

Load Case 2: axial dead load plus wind load (1.4 W + 1.25D + 0.5 S)

Factored wind load (w_f) 0.513 kN/m per stud

Factored axial load (P_f) 29.2 kN per stud

Maximum moment (M_f) at centre of stud

$$\begin{aligned}M'_f &= \frac{w_f \ell^2}{8} + \frac{1}{2} P_f \times \frac{d}{6} \\ &= 4.39 \text{ kN}\cdot\text{m} \quad \text{per stud} \\ M_f &= 5.17 \text{ kN}\cdot\text{m} \quad \text{per stud}\end{aligned}$$

Combined loading:

$$\begin{aligned}\frac{P_f}{P_r} + \frac{M_f}{M_r} &\leq 1.0 \\ &= 0.41 \leq 1.0 \quad (\text{Acceptable})\end{aligned}$$

Shear:

$$\begin{aligned}V &= w_f \times \frac{\ell}{2} \\ &= 1.95 \text{ kN} \leq 31.7 \text{ kN} \quad (\text{Acceptable})\end{aligned}$$

Deflection (W + D + 0.5S):

Wall finishes, in this case OSB and lumber siding, are not brittle or subject to cracking. Acceptable total load deflection criteria is span/180 = 42 mm. Deflection is calculated at mid-span of the studs. In this Tall Wall example and the stud tables in Section 2, the deflections incorporate the deflections caused by the offset axial loads. The deflections from the wind loads and axial loads are amplified to account for the $P\Delta$ effect. These are conservative assumptions for determining stud deflection.

Specified wind load (w_s) = 0.275 kN/m per stud

Specified axial dead load (P_s) = 25.0 kN per stud

$$\begin{aligned}\Delta_T &= \text{deflection from wind} + \text{deflection from eccentric load} \\ &= \frac{5w_s \ell^4}{384EI} + \frac{P_s e \ell^2}{16EI} \\ &= 14.5 \text{ mm}\end{aligned}$$

Δ_A = amplified deflection to account for $P\Delta$ effect

$$\begin{aligned}&= \Delta_T \left[\frac{1}{1 - \frac{P_s}{P_E}} \right] \\ &= 16.7 \text{ mm} < 42 \text{ mm} \quad (\text{Acceptable})\end{aligned}$$

Load Case 3: axial load plus wind load (1.5 S + 1.25 D + 0.4 W)

Factored wind load (w_f)	= 0.147 kN/m	per stud
Factored axial load (P_f)	= 62.3 kN	per stud
Maximum moment (M'_f) at centre of stud		

$$\begin{aligned}M'_f &= \frac{w_f \ell^2}{8} + \frac{1}{2} P_f \times \frac{d}{6} \\ &= 2.54 \text{ kN}\cdot\text{m} \quad \text{per stud} \\ M_f &= 3.76 \text{ kN}\cdot\text{m} \quad \text{per stud}\end{aligned}$$

Combined loading:

$$\begin{aligned}\frac{P_f}{P_r} + \frac{M_f}{M_r} &\leq 1.0 \\ &= 0.6 \leq 1.0 \quad (\text{Acceptable})\end{aligned}$$

Deflection (S + D + 0.4W):

Specified wind load (w_s) =	= 0.11 kN/m	per stud
Specified axial dead load (P_s) =	= 39.9 kN	per stud

$$\begin{aligned}\Delta_T &= \text{deflection from wind + deflection from eccentric load} \\ &= \frac{5w_s \ell^4}{384EI} + \frac{P_s e \ell^2}{16EI} \\ &= 10.3 \text{ mm}\end{aligned}$$

Δ_A = amplified deflection to account for P Δ effect

$$\begin{aligned}&= \Delta_T \left[\frac{1}{1 - \frac{P_s}{P_E}} \right] \\ &= 13.0 \text{ mm} < 42 \text{ mm} \quad (\text{Acceptable})\end{aligned}$$

Results:

Use 44 x 286 mm (1-3/4 x 11-1/4 in) TEMLAM™ 2.0E spaced at 610 mm.

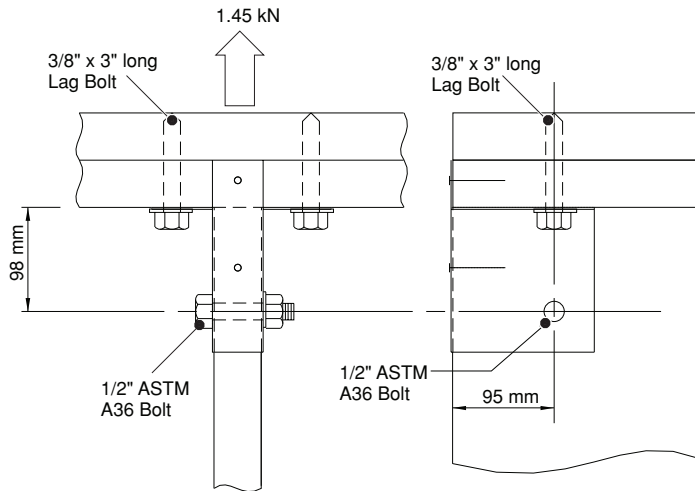
Other considerations:

- 1) Ensure that walls are laterally braced to prevent buckling about the narrow stud axis. The tongue and groove siding on the wall exterior, the OSB sheathing on the wall interior and the full depth blocking at 1.2 m will provide adequate bracing. For additional information on lateral bracing contact the stud manufacturer.
- 2) For wall segments used as shearwalls ensure all edges of sheathing are blocked. Blocking at 1.2 m intervals will provide edge support for all shearwall panels.

3.3 Stud Connection Design

Stud to wall plate connections must be designed to resist the uplift force on the stud and the wind loads resulting from the wind pressures/suctions on the face of the wall. For this project, special stud anchors were designed for the stud to plate connections. The top plate anchor is shown in Figure 3.6. TEMLAM™ 2.0E studs have the same specific gravity as Douglas-Fir.

Figure 3.6
Stud to top plate
connection



Load information

Factored uplift load at the eave (wind load – 0.9 roof dead load)

Critical wind uplift will be at the corner of the building  Figure 17

$$y = \text{end zone width} \\ = 6.18 \text{ m}$$

End Zone

$$C_p C_g = -2.0 \text{ windward side of roof} \\ = -1.0 \text{ leeward side of roof}$$

$$C_{pi} = 0.3$$

$$C_{gi} = 2$$

$$C_e = 0.7$$

Wind uplift at eave

$$= 15.88 \text{ kN/m}$$

Factored dead load at eave

$$= 15.0 \text{ kN/m} \times 0.9 \\ = 13.5 \text{ kN/m}$$

Net uplift at eave

$$= 2.4 \text{ kN/m}$$

Uplift load/stud

$$= 2.4 \times 0.61 \\ = 1.45 \text{ kN}$$

Wind pressures on stud

$$= \text{stud shear load (pg 46)} \\ = 1.95 \text{ kN}$$

Uplift resistance

Top plate connected to stud anchor with lag screws

Two 3/8 in dia. x 3 in long lag screws

$$P_{rw} = P'_{rw} L_t n_F K' J_E \quad \boxed{\text{WDM}}$$

Length of threaded portion, L_t , in top plate

$$\begin{aligned} L_t &= L/2 + 12.7 - \text{tip} \\ &= 50.8 - 9.5 \\ &= 41.3 \text{ mm} \end{aligned}$$

$$n_F = 2$$

$$K_D = 1.15 = K'$$

$$P'_{rw} = 72 \text{ N/mm}$$

$$P_{rw} = 6.84 \text{ kN} > 1.45 \text{ kN} \quad (\text{Acceptable})$$

Stud anchor connected to stud with single bolt loaded in double shear parallel to the grain

One 1/2 in dia. bolt

$$P_r = P'_r n_s n_F K' J' \quad \boxed{\text{WDM}}$$

Member end distance = 98 mm = 7.71 bolt diameters

$$\begin{aligned} J_L &= 1.0 @ 10 \text{ dia.} \\ &= 0.75 @ 7 \text{ dia.} \\ &= 0.81 @ 7.71 \text{ dia.} \\ &= J' \end{aligned}$$

$$K_D = 1.15 = K'$$

For 44 mm thick member, double shear, steel side plate

$$P'_r n_s = 8.84 \text{ kN}$$

$$P_r = 8.23 \text{ kN} > 1.45 \text{ kN} \quad (\text{Acceptable})$$

Resistance to wind pressures/suctions on the wall

Top plate connected to stud anchor with lag screws loaded perpendicular to the grain

Two 3/8 in dia. x 3 in long lag screws with steel side plate.

$$Q_r = Q'_r n_{Fe} n_R K' \quad \boxed{\text{WDM}}$$

Length of penetration, L_p , in top plate

$$\begin{aligned} L_p &= \text{length of lag screw} - \text{thickness of washer and steel in anchor} - \text{tip} \\ &= 76 - 9 - 9.5 \\ &= 57.5 \text{ mm} \end{aligned}$$

$$n_{Fe} = 1$$

$$n_R = 2$$

$$K_D = 1.15 = K'$$

$$Q'_r = 1.63 \text{ kN}$$

$$Q_r = 3.75 \text{ kN} > 1.95 \text{ kN} \quad (\text{Acceptable})$$

Stud anchor connected to stud with single bolt loaded in double shear loaded perpendicular to the grain

One 1/2 in dia. bolt

Member edge distance = 95 mm = 7.5 dia. > 4 dia. (Acceptable)

$$Q_r = Q'_r n_s n_F K' J_R$$

$$n_F = 1$$

$$K_D = 1.15 = K'$$

For 44 mm thick member, double shear, steel side plate

$$Q'_r n_s = 3.67 \text{ kN}$$

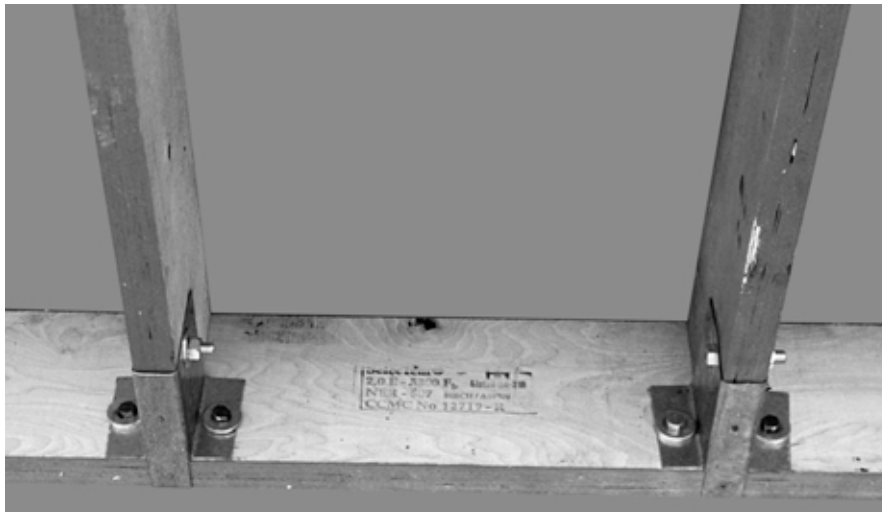
$$Q_r = 4.22 \text{ kN} > 1.95 \text{ kN} \quad (\text{Acceptable})$$

Results:

Stud anchor connections are adequate to resist the stud uplift and pressure/suction loads.

Other considerations:

- 1) Steel in stud anchor must be checked to ensure the anchor is capable of transferring the loads.
- 2) Stud to bottom plate anchor must also be checked. In this project, similar anchors were used at the top and bottom of the studs. The weight of the wall is beneficial to the connection at the bottom of the stud.
- 3) The connections between the roof framing and the top plate must be capable of resisting the uplift loads and the wind pressures/suctions. A load path must be detailed to ensure that the wind pressures/suctions, on the face of the wall, are resisted by the roof diaphragm acting in the plane of the roof sheathing.



3.4 Shearwall Design

The Crestbrook Value Added Centre uses a system of diaphragms and shearwalls to resist the lateral loads. Wind pressures and suctions on the north and south end walls of the buildings are resisted by the end wall studs which transfer half of the wind load into the foundation and the other half to the roof diaphragm. The roof diaphragm acts as a deep beam and transfers the wind loads into east and west walls along Gridlines G and M. The walls on gridlines G and M must be designed as shearwalls to ensure that they are capable of transferring the shear loads at the eave level into the foundation at the base of the wall.

3.4.1 Lateral Load Path and Overturning

The diaphragm load on the roof is assumed to be uniformly distributed along the top of the wall plate. This load is transferred through the effective shearwall segments to the foundation. All of Wall G is sheathed with OSB sheathing with only 3 door openings to reduce the shear capacity – see Figure 3.7. Therefore, most of the wall can be considered capable of transferring lateral loads.

A shearwall segment is defined as a section of a shearwall with uniform construction that forms a structural unit designed to resist lateral forces parallel to the plane of the wall. The wall segments around openings are not considered as part of the shearwall. As well, a wall section where the height of the wall is more than 3.5 times greater than the length of the segment is considered too narrow to carry load. This means there are three potential shearwall segments in Wall G as illustrated in Figure 3.7.

The wall sheathing nailed to the studs transfers the shear load from the top of the wall to the bottom of the wall. The overturning of each shearwall segment is resisted by dead loads on the wall segment and chords at the ends of the segments designed to transfer tension and compression forces into the foundation. Shearwall chords acting in tension require hold-down connections to the foundation. Where possible, wall geometry may be chosen to avoid using hold-down connections.

Load Information

Lateral loads

The factored roof diaphragm reaction at Wall G is 63 kN resulting from wind loads on the existing structure and the new Value Added Centre. The wall length is 53.9 m and the distributed diaphragm load along the top of the wall is 1.17 kN/m.

Dead loads

In wind load analysis, 90% of the specified dead load may be used to resist overturning. Since the roof dead load was considered to resist wind uplift, it will not be considered to resist overturning. Only the dead load of the wall will be considered in the overturning calculation.

Specified weight of wall = 0.4 kPa

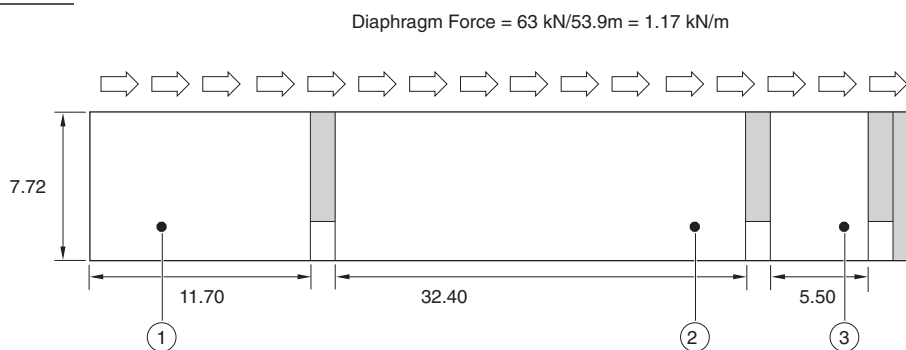
Wall height = 7.72 m

Factored weight of the wall at the base of the wall

$$= 0.9 \times 0.4 \times 7.72$$

$$= 2.78 \text{ kN/m}$$

Figure 3.7
Wall G showing
shearwall
segments

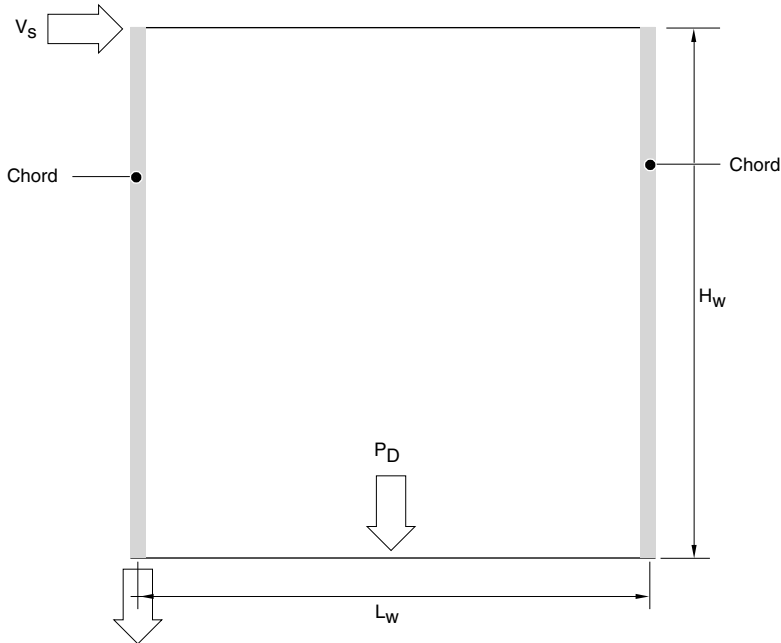


Load paths

Each shearwall segment must be considered separately. In this analysis, all shearwall segments are constructed in the same manner. Due to the low aspect ratio, shear deformation is dominant and each shearwall segment is assumed to have the same stiffness per unit length and the load in each segment is assumed to be proportional to the length of the segment.

Figure 3.8 shows a free body diagram for a shearwall segment. The sheathed panels above the openings are conservatively ignored in the shearwall design.

Figure 3.8
Free body
diagram of a
shearwall
segment



From static equilibrium

$$R_f = \frac{M_{\text{overturning}} - M_{\text{resisting}}}{L_w}$$

Where:

R_f = Hold-down force (positive is tension, negative is compression)

$M_{\text{overturning}}$ is the overturning moment

$$= V_s \times H_w$$

$M_{\text{resisting}}$ is the resisting moment

$$= P_D \times L_w / 2$$

L_w = The length of the shearwall segment

H_w = The height of the shearwall
= 7.72 m

$$V_s = \text{Load on the shearwall segment} = V_T \frac{L_w}{\sum L_w}$$

V_T = Total shear load on the shearwall
= 63 kN

P_D = Total factored dead load on the shearwall segment
= 2.78 kN/m \times L_w

Option 1 – 3 shearwall segments

$$\begin{aligned}\Sigma L_w &= 11.7 + 32.4 + 5.5 \\ &= 49.6 \text{ m}\end{aligned}$$

Segment	Length	Overturning Moment		Resisting Moment		R _f kN
	L _w m	V _s kN	V _s H _w kN•m	P _D kN	P _D L _w /2 kN•m	
1	11.7	14.9	115	32.5	190	-6.5
2	32.4	41.2	318	90.0	1460	-35.2
3	5.5	7.0	53.9	15.3	42.0	2.14

Option 2 – Only consider segments 1 and 2 as resisting lateral load

$$\begin{aligned}\Sigma L_w &= 11.7 + 32.35 \\ &= 44.1 \text{ m}\end{aligned}$$

Segment	Length	Overturning Moment		Resisting Moment		R _f kN
	L _w m	V _s kN	V _s H _w kN•m	P _D kN	P _D L _w /2 kN•m	
1	11.7	16.7	129	32.5	190	-5.2
2	32.4	46.3	357	90.0	1460	-34.0

In option 2, hold-downs would not be required. Base shearwall design on Option 2.

Results:
Only consider shearwall segments 1 and 2 in shearwall design.

Other considerations:

- 1) The top plate of the shearwall must be designed as a drag strut to transfer the diaphragm shear loads into the shearwall segments. See Section 3.4.5.

3.4.2 Shear Panel Design

Shear panels are 9.5 mm thick OSB nailed with 2 in common nails at 150 mm at panel edges and 300 mm at interior framing members. Alternatively, nailed plywood sheathing could be used for shear panels. OSB and plywood sheathing of the same thickness have equivalent shearwall shear capacity when nailed with the same size and number of nails. Panels are applied horizontally and blocking provides a nailing surface for all panel edges.

Shearwall capacity is given for 2 in nails used with 9.5 mm sheathing. Use capacity for D. Fir framing.

Factored shear resistance of shearwall segments is 4.35 kN/m



Factored shear load

$$\begin{aligned} &= V_T / \Sigma L_w \\ &= 63 / 44.1 \\ &= 1.43 \text{ kN/m} < 4.35 \text{ kN/m} \quad (\text{Acceptable}) \end{aligned}$$

Results:

The interior sheathing consisting of 9.5 mm thick OSB nailed with 2 in common nails at 150 mm at the panel edges and 300 mm at interior framing members provides adequate shear resistance for lateral loads.

3.4.3 Chord Design

Typically, the chords of each shearwall segment will act in compression and tension alternately depending on the direction of the lateral load. Studs are usually doubled at the ends of the shearwall segments to act as the chords. The double member chord must be capable of resisting the chord force, roof gravity loads and wind loads on the face of the stud.

In the example given, there are no tie downs required, therefore there will not be tension in the chord, only compression.

Chord force

When calculating the compression force in the shearwall chord resulting from the shear force, the weight of the wall does not need to be considered. The weight of the wall is resisted by all of the studs in the shearwall segment. The design of the studs acting as chords must also consider the gravity loads and wind pressures/suctions on the stud.

Useful length of wall = $L_w - 300$ mm to allow room for connections

$$R_{fc} = V_s \times H_w / (L_w - 300)$$

Segment 1

$$= 11.3 \text{ kN}$$

Segment 2

$$= 11.1 \text{ kN}$$

Stud design

For studs used as a chord, check stud capacity considering extra axial load from chord.

Wind load on the face of the stud:

Since design is considering wind loads on multiple surfaces of the structure, use Figure I-7 of the Structural Commentaries to the NBCC – wind blowing on the end wall.

Calculations are per double stud

$$C_p C_g = 0.9$$

Wind principal load

Snow companion load

$$1.4W + 1.25D + 0.5S$$

$$w_f = 0.296 \text{ kN/m}$$

$$P_f = 29.2 \text{ kN} + 11.3 \text{ kN} \\ = 40.5 \text{ kN}$$

$$P_r = 2 \times 132 \\ = 265 \text{ kN}$$

$$M_r = 2 \times 27.8/1.04 \\ = 53.5 \text{ kN}\cdot\text{m}$$

Combined loading:

$$\frac{P_f}{P_r} + \frac{M_f}{M_r} \leq 1.0$$

$$= 0.22 \leq 1.0 \quad (\text{Acceptable})$$

Deflection $W + D + 0.5S$:

$$w_s = 0.159 \text{ kN/m}$$

$$P_s = 25.0 + 0.4 \times 11.3/1.4 \\ = 31.8 \text{ kN}$$

$$\Delta_A = 5.89 \text{ mm} < 42 \text{ mm} \quad (\text{Acceptable})$$

Snow principal load

Wind companion load

$$0.4W + 1.25D + 1.5S$$

$$w_f = 0.084 \text{ kN/m}$$

$$P_f = 62.3 \text{ kN} + 0.4 \times 11.3/1.4 \\ = 65.5 \text{ kN}$$

$$P_r = 265 \text{ kN}$$

$$M_r = 53.5 \text{ kN}\cdot\text{m}$$

Combined loading:

$$\frac{P_f}{P_r} + \frac{M_f}{M_r} \leq 1.0$$

$$= 0.28 \leq 1.0 \quad (\text{Acceptable})$$

Deflection: $0.4W + D + S$:

$$w_s = 0.063 \text{ kN/m}$$

$$P_s = 39.9 + 0.75 \times 11.3/1.4 \times 0.4 \\ = 42.3 \text{ kN}$$

$$\Delta_A = 5.00 \text{ mm} < 42 \text{ mm} \quad (\text{Acceptable})$$

Results:

Two 44 x 286 mm (1-3/4 x 11-1/4 in) Temlam™ 2.0E studs are acceptable as a shearwall chord.

Other considerations:

- 1) Studs around openings must be designed to resist the additional loads imposed at the openings – See Section 3.5.

3.4.4 Anchor Bolt Design

The anchor bolts which connect the base plate to the foundation, must be designed to resist the wind uplift force on the wall, the wind loads resulting from the wind pressures/suctions on the face of the wall and the wind shearwall shear forces acting parallel to the plane of the wall. For this project, 5/8 in dia. anchor bolts were used with a minimum embedment of 127 mm into the concrete. Temlam™ 2.0E base plates have the same specific gravity as Hem-Fir and Tembec recommends using Hem-Fir connection design values for this product.

Load information

Factored uplift load at the eave (pg 48)

$$\begin{aligned} &= (\text{wind load} - 0.9 \text{ roof dead load}) \\ &= 2.4 \text{ kN/m} \end{aligned}$$

Wind pressures (pg 48)

$$\begin{aligned} &= 1.95/0.61 \\ &= 3.20 \text{ kN/m} \end{aligned}$$

Lateral shear loads along shearwall (pg 54)

$$= 1.43 \text{ kN/m}$$

Uplift resistance

70 x 70 x 6 mm thick square washers resist wind uplift forces

Check bearing of washers on the wall plate.

Bearing area:

$$Q_r = \phi F_{cp} A_b K_B K_{Zcp}$$

$$\begin{aligned} A_b &= 70 \times 70 - \pi \times 18^2/4 \\ &= 4650 \text{ mm}^2 \end{aligned}$$

$$K_B = 1.13$$

$$K_{Zcp} = 1.15$$

$$Q_r = 40.2 \text{ kN}$$

Anchor bolt spacing for uplift:

$$\begin{aligned} &= 40.2/2.4 \\ &= 16.8 \text{ m} \end{aligned}$$

Resistance to wind pressures/suctions on the wall

44 mm bottom plate; 5/8 in dia. anchor bolt; plate loaded perpendicular to grain, anchor bolt embedded 100mm in concrete

$$Q_r = Q'_r n_s n_f K^1 J^1 \quad \boxed{\text{WDM}}$$

where:

$$Q'_r n_s = 3.99 \text{ kN}$$

$$n_f = 1$$

$$K^1 = 1.15$$

$$J^1 = 1$$

$$Q_r = 4.59 \text{ kN}$$

Anchor bolt spacing for face loads:

$$= 4.59/3.2$$

$$= 1.4 \text{ m} \quad (\text{Governs})$$

Resistance to lateral shear loads parallel to the wall

44 mm bottom plate; 5/8 in dia. anchor bolt; plate loaded parallel to grain, anchor bolt embedded 100mm in concrete

$$P_r = P'_r n_s n_f K^1 J_L J_R \quad \boxed{\text{WDM}}$$

where:

$$P'_r n_s = 6.74 \text{ kN}$$

$$n_f = 1$$

$$K^1 = 1.15$$

$$J_L = 1$$

$$J_R = 1$$

$$Q_r = 7.75 \text{ kN}$$

Anchor bolt spacing for lateral loads:

$$= 7.75/1.43$$

$$= 5.4 \text{ m}$$

Face loads will govern the spacing of the anchor bolts. Use 1.22 m anchor bolt spacing to have an anchor bolt every 2 studs.

Results:

Use 5/8 in dia. anchor bolts with 70 x 70 mm plate washers spaced at 1.22 m.

Other considerations:

- 1) The resistance of the concrete to the connection forces needs to be checked.
- 2) When anchor bolts are widely spaced, the bending capacity of the wall plate needs to be checked in both the strong and weak axis.

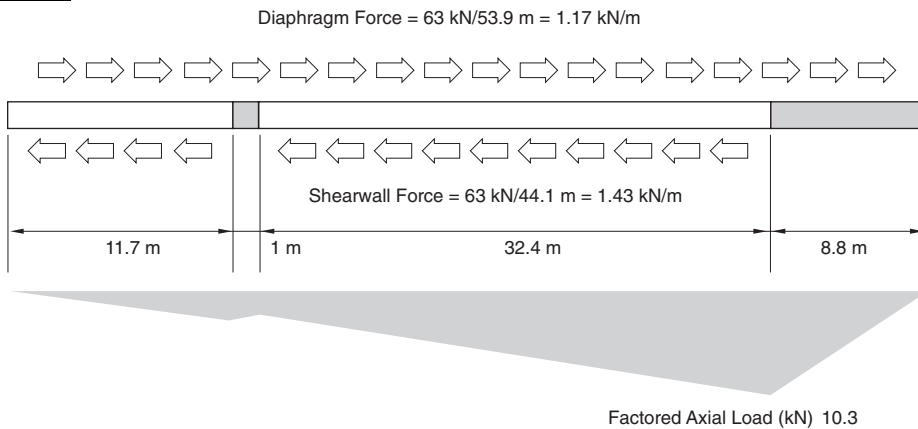
3.4.5 Drag Strut Design

A drag strut – also known as a collector, tie or diaphragm strut - is a diaphragm or shearwall boundary element parallel to the applied load that collects and transfers diaphragm shear forces to the shearwall segments. Typically the wall top plate acts as the drag strut and the connections in the top plate must be designed to resist the drag strut axial tension or axial compression forces.

The south 8.8 m segment of Wall G was not designed as a shearwall segment. Therefore, the diaphragm shear force at the south end of the wall has to be transferred to the shearwall segments at the north end of the wall. Figure 3.9 is a force diagram which illustrates the drag strut forces along wall G.

The maximum drag strut force is 10.3 kN. Since the shear force can occur from either the north or south direction, this can be either a tension force or a compression force. The maximum tension or compression stress in a single plate is 0.82 MPa. By observation, a single 44 x 286 mm member is capable of resisting this force. The plate members must be connected to provide continuity.

Figure 3.9
Drag strut forces along wall G



Drag strut connection

Stagger the butt joints in each of the top chord members and nail the top plates together. Use 2 rows of 3-1/2 in common nails.

$$\phi n_u J_y = 1.02 \text{ kN} \quad \text{WDM}$$

$$K_D = 1.15$$

Capacity per nail

$$= 1.17 \text{ kN}$$

Number of nails/row

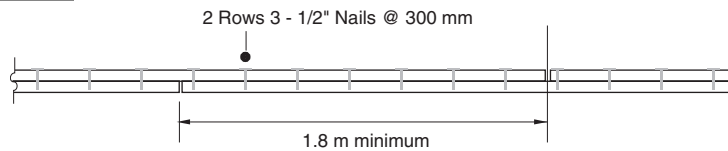
$$= 10.3 / (2 \times 1.17)$$

$$= 4.40 \text{ (5 nails)}$$

Space nails at 300 mm.

Stagger end joints in the top plate 1.8 m.

Figure 3.10
**Top plate
designed as
drag strut**



Results:

Design the wall top plate to act as a drag strut. Stagger end joints in the wall plate members a minimum of 1.8 m. Nail plates with 2 rows of 3-1/2" nails spaced at 300 mm.

Other considerations:

- 1) The wall top plate is often used as the diaphragm chord. The splice connections in the top plate should be designed for the most critical of the diaphragm chord force or the drag strut force.

3.5 Design of Members and Connections Around the Wall Opening

Loads must be transferred around the openings in a wall. The members and their connections listed below must be designed for the following load cases:

Member	Load considerations
Lintel over opening	gravity loads above the opening
	uplift loads above the opening
	wind pressures and suctions acting on the face of the wall and door or window
Jack post stud	gravity reactions from lintel
King post stud	loads for a typical stud
	chord forces if the opening is adjacent to a shearwall segment
	lateral load reactions from the lintel
	uplift reactions from the lintel

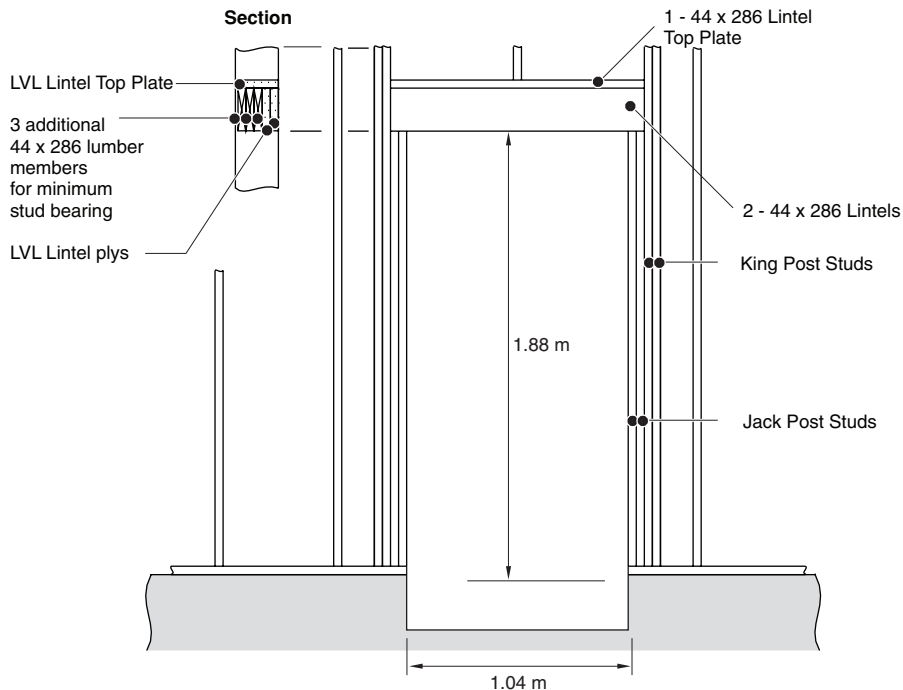
This design example will focus on the door opening near the north end of Wall G – see Figure 3.1. The opening is 1.04 m wide x 1.88 m high. At this location, the wall supports trusses spanning 41.8 m and there are shearwall segments either side of the opening. The opening is far enough away from the north end of the building to use the reduced wind loads for members away from building corners.

3.5.1 Lintel Member and Connection Design

Figure 3.11 illustrates the opening and the framing around the opening. A portion of the axial loads and wind loads is resisted directly by the studs adjacent to the opening. The lintel has to resist the loads from the stud supported on the lintel.

The lintel is LVL 2-Ply with an LVL lintel top plate – see Figure 3.11. All of the lintel members are 44 x 286 mm Temlam™ 2.0E.

Figure 3.11
Framing around
the opening



2-Ply lintel design to resist gravity loads and uplift loads

From Table 3.1 (pg 41):

Total factored gravity load is 62.3 kN

Specified snow load is 33.1 kN

For the factored gravity load acting as a point load in the centre of the span:

$$M_f = 16.2 \text{ kN}\cdot\text{m}$$

$$K_H = 1$$

$$\begin{aligned} M_r &= 24.2/1.04 \times 2 \\ &= 46.5 \text{ kN}\cdot\text{m} > 16.2 \text{ kN}\cdot\text{m} \quad (\text{Acceptable}) \end{aligned}$$

$$V_f = 31.2 \text{ kN}$$

$$K_D = 1$$

$$\begin{aligned} V_r &= 31.7/1.15 \times 2 \\ &= 55.1 \text{ kN} > 31.2 \text{ kN} \quad (\text{Acceptable}) \end{aligned}$$

Deflection

$$P_s = 33.1 \text{ kN}$$

$$\text{span} = 1.04 \text{ m}$$

$$\Delta < 1 \text{ mm} \quad (\text{Acceptable})$$

Check bearing

$$\text{Bearing reaction} = 31.2 \text{ kN}$$

$$Q_r = \phi F_{cp} A_b K_B K_{zcp} \quad \text{CSA 086.1 Supplement, 13.4}$$

Bearing width for 2-ply lintel

$$\begin{aligned} &= 2 \times 44 \\ &= 88 \text{ mm} \end{aligned}$$

Assume 2 jack post studs

Bearing length

$$\begin{aligned} &= 2 \times 44 \\ &= 88 \text{ mm} \end{aligned}$$

$$K_B = 1$$

$$K_{zcp} = 1$$

$$Q_r = 44.8 \text{ kN} > 31.2 \text{ kN} \quad (\text{Acceptable})$$

Factored uplift load

$$\begin{aligned} &= 2.4 \text{ kN/m} \times 0.61 \\ &= 1.45 \text{ kN} \end{aligned}$$

Uplift reaction on the 2-ply beam = 0.73 kN

End-nail the king post stud to the 2-ply lintels using 3-1/2 in. common nails

Use nail design values for D. Fir lumber.

Resistance per nail

$$N_r = \phi N_u J_F \quad \text{CSA 086.1 10.9.4}$$

Factor for end-nailing $J_E = 0.67$

Wind load $K_D = 1.15$

$$N_r = 0.79 \text{ kN}$$

Two nails required – better to use two nails per ply.

End nail with two 3-1/2 in nails each ply of lintel

Results:

Use a 2-ply 44 x 286 mm Temlam™ 2.0E lintel. Support the lintel on two jack post studs at each end. End nail the king post stud to the lintel using two 3-1/2 in nails per ply.

Other considerations:

- 1) Lintel plys should be nailed together in accordance with the manufacturer's recommendations.
- 2) Use filler members to provide full support to the lintel top plate-see Figure 3.11

Lintel top plate designed to resist wind pressures and suctions on the face of the wall

Lateral loads – wind loads away from the corner of the building

$$C_p C_g = -1.75 \quad \text{NBCC Figure I8}$$

$$C_e = 0.7$$

$$C_{gi} = 2.0$$

$$C_{pi} = \pm 0.3$$

Factored load for strength calculations = 0.76 kPa

Specified load for deflection calculations = 0.41 kPa

Tributary area for lintel

$$\begin{aligned} &= 7.62/2 \times 0.61 \\ &= 2.32 \text{ m}^2 \end{aligned}$$

For strength calculations load = 1.77 kN

For deflection calculations load = 0.95 kN

For the wind suction acting as a point load in the centre of the 1.04 m span beam:

$$M_f = 0.46 \text{ kN}\cdot\text{m}$$

$$K_H = 1$$

$$\begin{aligned} M_r &= 27.8/1.04 \\ &= 26.7 \text{ kN}\cdot\text{m} > 0.46 \text{ kN}\cdot\text{m} \quad (\text{Acceptable}) \end{aligned}$$

$$V_f = 0.88 \text{ kN}$$

$$K_D = 1.15$$

$$V_r = 31.7 \text{ kN} \quad (\text{Acceptable})$$

Deflection

Using conservative assumption of

$$P_s = 0.95 \text{ kN}$$

$$\text{span} = 1.04 \text{ m}$$

$$\Delta < 1 \text{ mm} \quad (\text{Acceptable})$$

Lateral reaction on the lintel top plate = 0.88 kN

End-nail the king post stud to the lintel top plate using 3-1/2 in common nails

Resistance per nail

$$N_r = 0.79 \text{ kN}$$

2 nails required

End nail with two 3-1/2 in common nails

Results:

Use a 44 x 286 mm Temlam™ 2.0E lintel top plate. End nail the king post stud to the lintel top plate using two 3-1/2 in nails per ply.

3.5.2 Jack Post Stud Design

Factored Axial Load/Stud = 15.6 kN

Stud Length = 1.88 m

P_r for 1.88 m stud = 293 kN

By observation, 2-jack post studs each end of lintel are adequate

3.5.3 King Post Member and Connection Design

Check the capacity of a double king post stud. The king post stud must be designed to resist the combined uplift and lateral loads from the lintel and the combined axial and lateral loads from the wind loads on the face of the wall, the shearwall chords, and the lintel.

The lintel is at 1/4 the height of the stud. Lateral load is 0.88 kN. Additional moment caused by wind load on the face of the studs away from the opening must be considered – See Section 3.4.3 (pg 54)

Calculations are per double stud

$$\begin{aligned} M_f &= 1.25 + 0.296 \times 7.59^2/8 \\ &= 3.38 \text{ kN}\cdot\text{m} \end{aligned}$$

$$K_H = 1$$

$$M_r = 53.5 \text{ kN}\cdot\text{m}$$

$$\begin{aligned} T_f &= 0.88 + 1.77 \\ &= 2.65 \text{ kN} \end{aligned}$$

$$\begin{aligned} T_r &= 2 \times 359 \\ &= 718 \text{ kN} \end{aligned}$$

$$\frac{T_f}{T_r} + \frac{M_f}{M_r} \leq 1.0$$

$$= 0.1 < 1.0 \quad (\text{Acceptable})$$

$$\begin{aligned} V_f &= 0.75 \times 0.88 + 1.12 \\ &= 2.00 \text{ kN} \end{aligned}$$

$$K_D = 1.15$$

$$V_r = 2 \times 31.7$$

$$= 63.4 \text{ kN (Acceptable)}$$

Wind principal load

Snow companion load

1.4W + 1.25D + 0.5S

$$M_{wind} = 3.38 \text{ kN}\cdot\text{m}$$

$$P_f = 29.2 \text{ kN} + 11.4 \text{ kN}$$

$$= 40.5 \text{ kN}$$

$$P_r = 2 \times 132$$

$$= 265 \text{ kN}$$

$$M_r = 2 \times 278/1.04$$

$$= 53.5 \text{ kN}\cdot\text{m}$$

Combined loading:

$$\frac{P_f}{P_r} + \frac{M_f}{M_r} \leq 1.0$$

$$= 0.22 \text{ (Acceptable)}$$

Snow principal load

Wind companion load

0.4W + 1.25D + 1.5S

$$M_{wind} = 0.966 \text{ kN}\cdot\text{m}$$

$$P_f = 62.3 \text{ kN} + 0.4 \times 11.3 \text{ kN}/1.4$$

$$= 65.5$$

$$P_r = 265 \text{ kN}$$

$$M_r = 53.5 \text{ kN}\cdot\text{m}$$

Combined loading:

$$\frac{P_f}{P_r} + \frac{M_f}{M_r} \leq 1.0$$

$$= 0.27 \text{ (Acceptable)}$$

Connection

A double steel connection was developed similar to the connection shown in Figure 3.6. See Example Section 3.3 (pg 48).

Uplift capacity of connection:

Withdrawal capacity of lag screws = 6.8 kN

Shear capacity of bolt (44 mm thick member) = 8.23 kN

Note: shear capacity would be greater for the double stud

Uplift load = 2.65 kN < 6.8 kN (Acceptable)

Capacity of connection to resist wind loads on the face of the wall:

Lag screw capacity = 3.75 kN

Shear capacity of bolt (44 mm thick member) = 4.22 kN

Note: shear capacity would be greater for the double stud

Lateral load

$$= 1.77 + 0.66$$

$$= 2.43 \text{ kN} < 4.22 \text{ kN (Acceptable)}$$

Results:

Double the studs around the opening.
Use a double stud anchor to resist the stud uplift and pressure/suction loads.

3.6 Non-structural Considerations

3.6.1 Fire Resistance

The Crestbrook Facility is classified as a Group F Division 2, industrial medium hazard occupancy. All Group F Division 2 buildings over 1500 m² must be sprinklered regardless of construction.

NBCC 3.2.2.70

As per NBCC 3.2.2.70, the building is permitted to be of combustible construction. The roof does not require a fire resistance rating because the building is sprinklered. The walls do not require a fire resistance rating because the roof that they are supporting does not require a fire resistance rating. Fire tests at the National Research Centre in Ottawa have demonstrated that wood stud walls have the same or better fire resistance as sheet metal stud walls with the same wall finishes.

For more information on fire resistance of wood buildings, refer to CWC publication, *Fire Safety Design of Buildings*. Code requirements for buildings can be determined using the CWC's CodeCHEK software, available from the web site at www.wood-works.org.

3.6.2 Thermal Resistance

Wood is a good insulator compared to other structural materials. The cellular structure of wood traps air which results in its good insulating properties. Steel framing members conduct heat and cold and

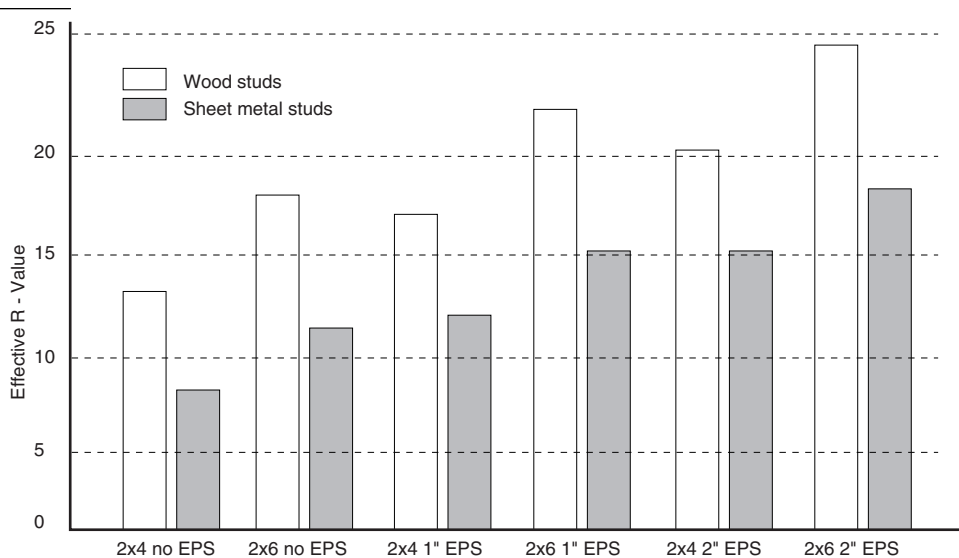
act as a thermal bridge through wall assemblies. This thermal bridging lowers the effective R-value or actual insulation value of the assembly.

As shown in Figure 3.12, sheet metal framing lowers the effective R-value of the cavity insulation by close to 50 percent while wood framing impacts the effective R-value by less than 10 percent. In other words, a 2 x 6 in. sheet metal frame wall would need to add 51 mm (2.0 in.) of foam insulation to achieve the same insulating value as a wood-frame wall with cavity insulation. This results in additional costs for the sheet metal system to provide the same thermal performance.

In this case, the R20 batt insulation in the wood stud wall provides an effective R-value of R18. A steel frame building, using non-loadbearing 2x4 sheet metal studs with R12 batt insulation and 2 in of EPS foam would have a lower effective R-value of R15 even though the insulation costs would be greater. The lower effective R-value would result in higher heating costs for the building.

For more information, refer to Canadian Wood Council at www.cwc.ca.

Figure 3.12
Wood vs. steel framing – effective insulation values



Source: National Energy Code for Houses 1995

www.cwc.ca

Canadian
Wood
Council

Conseil
canadien
du bois



BOISE[®]
Engineered Wood Products

JAGER
ENGINEERED WOOD PRODUCTS

**NORDIC**
ENGINEERED WOOD

LP[®]
BUILDING PRODUCTS